

1 **Vorticity recirculation and asymmetric generation at a**
2 **small headland with broadband currents**

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6 **Key Points:**

- 7 • At a 1 km scale headland (Pt. Sal CA), depth averaged vorticity varied $\pm 8f$ and
8 was asymmetrically related to along-headland flow.
- 9 • Vorticity also depends on flow acceleration, indicating short (2 h) adjustment timescale,
10 recirculation, and headland generation.
- 11 • Estimated potential vorticity across the headland indicates asymmetric vorticity
12 generation stronger for northward flow.

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Abstract

Fixed ADCP velocity measurements are used to investigate headland vorticity generation and recirculation in ~ 20 m depth around the small (~ 1 km) central California headland Pt. Sal. To reduce vorticity estimation noise, velocities are reconstructed from the first two EOF modes representing $\approx 73\%$ of the variance. Using fixed ADCPs, depth-averaged vorticity is estimated west and south of Pt. Sal. Only one west-location vorticity component is estimated, leading to negative vorticity bias for northward flow. The south location vorticity is consistent with estimates from parallel vessel transects on one day. The observed depth-averaged flow V was primarily along-bathymetric contours and varied ± 0.2 m s^{-1} across subtidal and tidal frequency bands. The depth-averaged normalized vorticity $\bar{\zeta}/f$ varied ± 8 across all frequency bands. Vorticity distributions are skewed with opposite sign at west and south locations, and $\bar{\zeta}/f < -1$ is more likely at the west location. At both locations, depth-averaged vorticity and velocity are inversely related, with relationship asymmetric with sign of V , indicating headland and farther upstream vorticity generation. Binned-mean $\bar{\zeta}/f$ depends on both V and its time-derivative, and indicates vorticity recirculation across the headland. The ~ 2 h vorticity adjustment timescale and the associated short excursion distances indicate vorticity generation between south and west locations. Potential vorticity changes across the headland are different for positive and negative V indicating headland asymmetric vorticity generation. Pt. Sal occupies a non-dimensional parameter space that is unique relative to other well studied headlands.

1 Introduction

Steady and tidal (oscillating) flows past topographic features such as headlands and islands lead to wake development and eddy shedding (*e.g.*, Signell & Geyer, 1991; Canals et al., 2009; MacKinnon et al., 2019), frontal development from flow separation (Farmer et al., 2002), and internal lee wave generation (*e.g.*, MacCready & Pawlak, 2001; Warner & MacCready, 2014; Voet et al., 2020). Strong relative vorticity ζ was observed for headland and island wakes with ζ/f of $O(1-10)$ (f is the Coriolis parameter) over a range of length-scales, from $O(0.1-10$ km) (*e.g.*, Wolanski et al., 1984; Canals et al., 2009; MacKinnon et al., 2019). Headland and island wakes can be important in the cross-shelf transport of larvae, sediment, and other tracers (*e.g.*, Roughan et al., 2005; George et al., 2015).

Previous modeling studies of wakes generated by steady flow around headlands and islands have mainly focused on obstructions with length-scales L of $O(10$ km), such as Pts. Arena and Reyes (Gan & Allen, 2002). For such headland length-scales, modeled wakes can extend significant distances downstream relative to the length-scale of the headland or island (Gan & Allen, 2002; Dong et al., 2007). Neglecting barotropic or baro-

50 clinic tides, about one third of Southern California Bight modeled eddy activity was at-
 51 tributed to island wakes (Dong & McWilliams, 2007). Large scale ($L \sim 10$ km) features
 52 and moderate flow rates ($U \sim 0.1$ m s⁻¹) generally result in a small Rossby number Ro
 53 ($= U/fL$) of $O(0.1)$. Stratification affects headland wakes and is quantified by the Burger
 54 number $Bu = (L_d/L)$, where the baroclinic deformation radius $L_d = Nh/f$ for water
 55 depth h and buoyancy frequency $N (= \sqrt{(-g/\rho_0)\rho_z})$, where ρ is density and z is the ver-
 56 tical coordinate). Vorticity generation increases with the Rossby number Ro and, for in-
 57 termediate Ro and Bu, decreases for increasing Bu (Castelao & Barth, 2006; Dong et
 58 al., 2007). The Ro dependence implies that, for a fixed headland and stratification, headland-
 59 generated vertical vorticity magnitude $|\zeta|/f$ depends on $|U|$ for steady flow but with vor-
 60 ticity and velocity having opposite signs as flow magnitude is reduced in shallower wa-
 61 ter where friction is larger.

62 Other headland wake studies have focused on tidal (*i.e.*, oscillatory) flow. For tidal-
 63 flow, vertical vorticity generation has been observed downstream of a headland (*e.g.*, Geyer
 64 & Signell, 1990). In a seminal paper, Signell & Geyer (1991) modeled unstratified tidal
 65 flow past a symmetric (Gaussian) headland to study the vorticity generation and evo-
 66 lution. The curl of the quadratic bottom stress is key to vorticity generation and dis-
 67 sipation, with a bottom-friction decay scale $t_{bf} = h/C_D U_0$ based on water depth h , drag
 68 coefficient C_D , and tidal velocity U_0 . Vorticity evolution depended on three non-dimensional
 69 parameters. The first nondimensional parameter is the headland aspect ratio (cross-shore
 70 to alongshore extent). Second, the frictional Reynolds number $Re_f = h/C_D L$ is the ra-
 71 tio between advection and quadratic bottom friction, and represents the vorticity decay
 72 length-scale relative to the headland scale L . Third, the Keulegan-Carpenter number $K_c =$
 73 $U_0/\omega L$, where ω is the tidal frequency, is the ratio of tidal excursion amplitude to the
 74 headland length-scale. Note, Signell & Geyer (1991) kept the tidal Rossby number U_0/fL
 75 fixed, also likely an important parameter. A fourth non-dimensional parameter, based
 76 on the others, is the ratio of frictional to tidal time-scale $\omega t_{bf} = Re_f/K_c$, which mea-
 77 sures whether vorticity is short- ($Re_f/K_c \ll 1$) or long-lived ($Re_f/K_c \gg 1$) relative
 78 to a tidal cycle. Note, Re_f/K_c also can be interpreted as the ratio of frictional to tidal
 79 length-scales. For $Re_f/K_c > 1$, the longer-lived vorticity can recirculate back across the
 80 headland as the tidal cycle switches, a situation which is not possible for steady flows
 81 (finite Re_f and $Re_f/K_c \ll 1$). Laboratory experiments of oscillating shallow water flow
 82 past a cylinder have enumerated the rich wake behavior over a large range of Re_f and
 83 K_c (*e.g.*, Lloyd et al., 2001). Tidal headland wake eddies were studied on a beach-nourishment
 84 generated (Stive et al., 2013) sandy headland with $L \sim 1000$ m, $h \sim 10$ m, and low
 85 aspect ratio. In both observations and models, significant but unspecified vorticity was
 86 generated every flood tide (Radermacher et al., 2017) with eddy intensity modulated by
 87 the spring-neap cycle. These eddies were short-lived (*i.e.*, less than a tidal cycle), sug-
 88 gesting $Re_f/K_c \lesssim 1$.

89 Baroclinic effects of tidal flows past $L \sim 1$ km headlands with large aspect ratio
 90 in deep water ($h \approx 200$ m) have been studied at the largely symmetric Three Tree Point
 91 (TTP, located in the Puget Sound) both with observations and models (Pawlak et al.,
 92 2003; Edwards et al., 2004; McCabe et al., 2006; Canals et al., 2009; Warner & MacCready,
 93 2014). As with $L \sim 1$ km scale barotropic headland studies, observed TTP ζ/f is of-
 94 ten relatively large, of $O(1)$. TTP vorticity is regularly tilted with respect to stratifica-
 95 tion (Canals et al., 2009) and short lived relative to the barotropic frictional decay scale
 96 t_{bf} , suggesting baroclinic mechanisms associated with tilted vorticity are significant in
 97 eddy decay (Pawlak et al., 2003). The baroclinic Froude number $Fr = U_0/Nd$, with
 98 N and obstruction height d , is an additional important nondimensional parameter rel-
 99 evant for both steady (*e.g.*, Dong et al., 2007) and oscillating (*e.g.*, MacCready & Pawlak,

2001) baroclinic wakes. For $Fr \ll 1$, flow travels around the obstacle, leading to flow separation and potentially eddy formation. As $Fr \approx 1$, flow transitions to going over the obstacle and can lead to lee wave generation (MacCready & Pawlak, 2001). As part of the Flow Encountering Abrupt Topography (FLEAT) experiment, wake processes around the island of Palau have been extensively studied (MacKinnon et al., 2019; Zeiden et al., 2019; Rudnick et al., 2019; Johnston et al., 2019; Merrifield et al., 2019; Voet et al., 2020). The Palau bathymetry is deep with large aspect ratio, similar to TTP, but with larger ($L \sim 10$ km) “headland” scale. Regional currents have both tidal, near-inertial, and lower frequency variability. Flows past the steep regional bathymetry can generate both nonlinear internal lee waves (Voet et al., 2020) and large-scale, high Ro vorticity, suggesting significant variability in Fr (Rudnick et al., 2019; MacKinnon et al., 2019; Zeiden et al., 2019).

Most locations cannot be neatly classified into pure steady or tidal flow, and instead have broadband flows, comprised of low frequency subtidal (time-scale > 33 h) plus tidal (diurnal and semidiurnal) flows of comparable magnitude. Vorticity generation with broadband flows is different from steady or oscillating flow alone (MacKinnon et al., 2019). For example, under combined strong steady and weak tidal flow, a series of same-signed vortices are likely generated and advected downstream. Aside from MacKinnon et al. (2019), most headland studies are for either oscillatory (tidal) or (quasi-) steady flow. Whether a steady-flow type relationship between local velocity and vorticity applies in broadband flows is unknown. For steady flows, headland flow response is different for symmetric and asymmetric obstacle (Castelao & Barth, 2006). Previously studied headlands at $L \sim 1$ km scale are also either largely symmetric (TTP) or have small aspect ratio (Zandmotor). Most modeling and laboratory studies use symmetric obstacles. In many cases, in particular on the US West Coast, headlands are asymmetric to the alongcoast flow, which may result in vorticity generation that is asymmetric with flow direction. These aspects of shallow small asymmetric headlands have not previously been studied. Lastly, strong anticyclonic vorticity $\zeta/f < -1$ will be centrifugally unstable (*e.g.*, Hoskins, 1974) and has low probability in open ocean observations and models (*e.g.*, Shcherbina et al., 2013a). However, the likelihood of strong anticyclonic versus cyclonic vorticity near a vorticity generating headland has not previously been studied.

Headland wake generation is naturally studied with vertical vorticity ζ . Whereas vorticity is straightforwardly estimated from numerical model solutions of headland or island wake flows (*e.g.*, Signell & Geyer, 1991), it is challenging to estimate observationally. Headland estimated vorticity used either shipboard ADCP surveys (Geyer & Signell, 1990; Pawlak et al., 2003; Canals et al., 2009; MacKinnon et al., 2019) or drifters (Pawlak et al., 2003). Yet, these studies were limited to measurements over, at most, a few semidiurnal cycles. To study headland vorticity generation with broadbanded currents, long vorticity timeseries that include subtidal and spring-neap tidal variability are required. This requires vorticity time-series estimated from fixed current meters, which has not previously been reported. Such longer-term vorticity observations at a headland under broadband currents can address the questions above and others such as: Is vorticity generated at a headland or is it advected from farther upstream? How much recirculation of vorticity occurs as along-headland flow switches sign?

Here, we address these headland vorticity related questions with a two-month (fall 2017) time-series of vorticity estimated at two locations across Pt. Sal, a small $O(1)$ km asymmetric headland with $O(1)$ aspect ratio located on the central California coast (Fig. 1), during the Inner-shelf Dynamics Experiment (Kumar et al., 2020). This region often has a headland wake as illustrated with a long-wave infrared (LWIR) surface temper-

149 ature and ADCP-measured flow (*e.g.*, Figure 1) with cool water (blue/green colors) stream-
 150 ing off Pt. Sal to the south-west and curves to the south-east. This wake orientation is
 151 consistent with the observed depth-averaged currents (black arrows). Headland vortic-
 152 ity generation and recirculation are studied statistically with vorticity estimated from
 153 fixed ADCP observations at two locations west and south of Pt. Sal. The study site, ve-
 154 locity filtering methods, and vorticity estimation technique are described in section 2.
 155 Statistical analysis of depth-averaged velocity and vorticity at the west and south loca-
 156 tions in isolation and comparison with vessel-based vorticity are given in section 3. In
 157 section 4, the local vorticity and velocity relationship is examined in regards to vortic-
 158 ity generation and recirculation. Potential vorticity in a steady flow paradigm is used
 159 to examine asymmetric headland vorticity generation (section 5). In the discussion, the
 160 relationship between vorticity recirculation and generation is examined (section 6.1) and
 161 Pt. Sal is placed in (dimensional and non-dimensional) context relative to other head-
 162 lands (section 6.2). Section 7 is a summary.

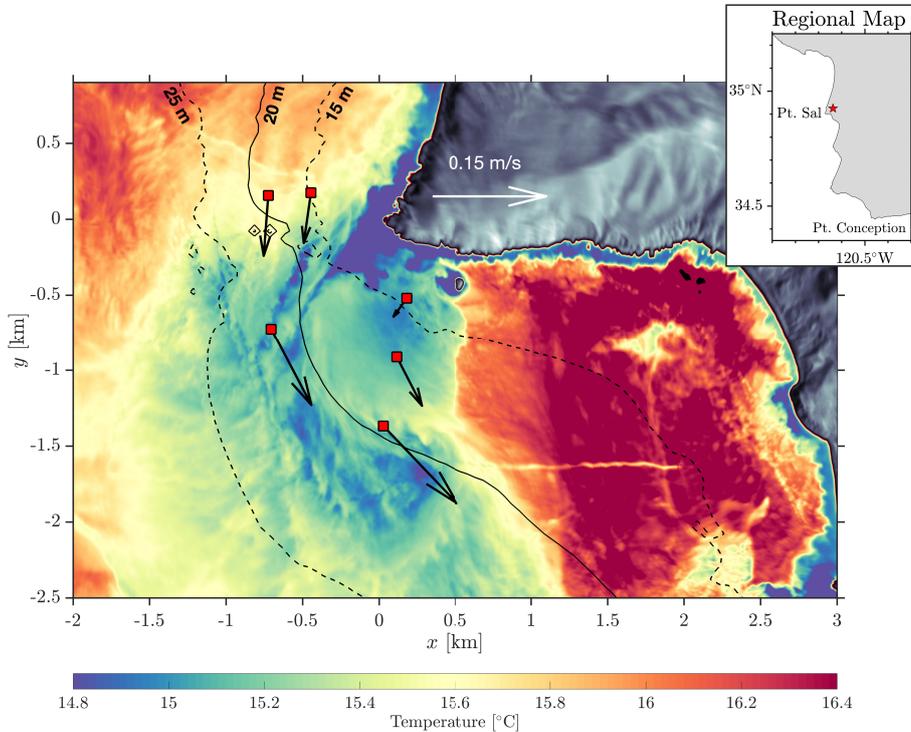


Figure 1. Long-wave infrared (LWIR) map of surface temperature around Pt. Sal, CA from the airborne Modular Aerial Sensing System (MASS, Melville et al., 2016). An Easting (x) and Northing (y) coordinate system is defined with origin at the tip of Pt. Sal (34.9030°N , 120.6721°W). Blue colors are cooler and red colors are warmer. Snapshot taken over a 3-minute window (11-Sep-2017, 10:41-10:44 PDT), overlaid with depth-averaged ADCP velocities (black arrows) which are time-averaged over same duration. The solid and dashed lines represent the 15, 20, and 25 m depth contours. (Inset) Map of Pt. Sal in the context of Pt. Conception.

2 Data and Methods

2.1 Experiment and regional description

In the fall of 2017, multiple institutions participated in the Inner Shelf Dynamics Experiment funded by an Office of Naval Research Departmental Research Initiative (ISDE) (Lerczak et al., 2019; Kumar et al., 2020). The experiment consisted of observations spanning 50 km alongshore on the Central CA coast, centered on the asymmetric rocky headland Pt. Sal (Fig. 1), over Sept to Oct 2017. An Easting (x) and Northing (y) coordinate system is defined with origin $(x, y) = (0, 0)$ m at the tip of Pt. Sal (34.9030°N , 120.6721°W). Northward of the point, the coastline is relatively straight, sandy beach interrupted with another small symmetric headland 3 km to the north. At Pt. Sal, the coast is rocky and the coastline bends approximately 120° . To the west of Pt. Sal, bathymetry contours are relatively compressed close to the point with several shoals and outcrops within 500 m west of the point, evidenced by cold water stream off of them (Fig. 1). From Pt. Sal, the rocky coastline extends eastward for 2.5 km before bending to the south where bathymetry contours are farther from shore and slopes are less steep.

Pt. Sal is located in an upwelling region, and the subtidal large-scale flow is primarily southward with episodic northward warm-water flow due to wind relaxation events, common during the fall months (Melton et al., 2009; Washburn et al., 2011; Suanda et al., 2016; Aristizábal et al., 2017). In addition, barotropic tides drive oscillating currents at Pt. Sal. Furthermore, semidiurnal nonlinear internal waves (NLIWs) regularly propagate into Pt. Sal (Colosi et al., 2018; Kumar et al., 2019; Feddersen et al., 2020), adding complexity. During the experiment, a broad array of 173 moorings and bottom landers were deployed from 100 m to 9 m depth along the 50 km stretch of coastline with many ADCPs, thermistors, and wave buoys in conjunction with multiple coastal high-frequency radars and meteorological stations (Kumar et al., 2020). In addition, two week-long intensive operations periods (IOPs) were conducted, one in mid-September (IOP1) and the other in mid-October (IOP2) with multiple vessels and aircraft sampling concurrently. Here, we only present a small subset of the experiment data that are focused on Pt. Sal. Additional information and studies related to the Inner Shelf Dynamics experiment are Lerczak et al. (2019); Spydell et al. (2019); McSweeney et al. (2020); Feddersen et al. (2020); Kumar et al. (2020).

2.2 Pt. Sal, CA moored and fixed location observations

Here we focus on an array of fixed location (bottom mounted, upward looking) ADCPs (Fig. 1, red squares) and thermistor moorings deployed (not shown) near Pt. Sal from September 1, 2017 through October 19, 2017 in water depths ranging from 13.5 to 25.0 m. This subset of locations was chosen for their high spatial resolution within a few km of the tip of Pt. Sal. Each thermistor mooring had 7–11 RBRsolo T thermistors with 1.5, 2, or 3 m vertical spacing (shallow moorings had higher vertical resolution) and a near bead RBR soloD pressure sensor. RBR soloT's have 0.002°C accuracy, RBR soloD's have 0.01 m accuracy, and both sampled at 1 Hz. Bottom mounted, upward-looking ADCPs measuring profiles of eastward and northward velocity (u, v) were co-located with a subset of the thermistor moorings. Here, z is the vertical coordinate positive upward and $z = 0$ m is the deployment time-averaged mean sea surface.

Most fixed location ADCPs were either 600 kHz or 1 MHz Nortek Aquadopp with vertical bin width Δz of 0.5–1 m. Two ADCPs were five-beam Nortek Signature1000 with $\Delta z = 0.5$ m. All ADCPs also had a pressure sensor used to estimate the tidal sea surface. ADCP velocity data within 2 m of the tidal sea surface or with low amplitudes

210 or correlations are removed. The lowest ADCP $\Delta z = 1$ m bin varies from 1 m to 2.6 m
 211 above the seabed, depending on bin size and blanking distance. The uppermost ADCP
 212 bin varies from $z = -3$ m to $z = -4$ m (relative to the mean sea level) due to the ± 1 m
 213 tidal range, the large (≈ 2.5 m at times) surface gravity waves, and side-lobe interfer-
 214 ence. All moored thermistor and ADCP data were averaged to a 1 minute sample in-
 215 terval and time-aligned from 13:00PDT 6-September to 06:00PDT 15-October, and here-
 216 after this time period is denoted the *analysis period*. For fluctuating flows, a low-pass
 217 time filter acts as a spatial filter at time-scales less than the dominant tidal velocity time-
 218 scale (Lumley & Terray, 1983a). Thus, to reduce aliasing of short length-scale (high hor-
 219 izontal wavenumber) variability in the vorticity calculations, moored ADCP velocities
 220 are low-pass filtered with a 2 h cutoff. For reference, this gives a 720 m cutoff length-
 221 scale for a steady 0.1 m s^{-1} current. Velocity data are then interpolated onto fixed ver-
 222 tical z levels at $\Delta z = 1$ m intervals, where $z = 0$ m is the mean tidal water level. This
 223 allows estimation of horizontal velocity gradients at a particular z level.

2.2.1 Vertical cEOF velocity reconstruction and depth-averaged statis- tics

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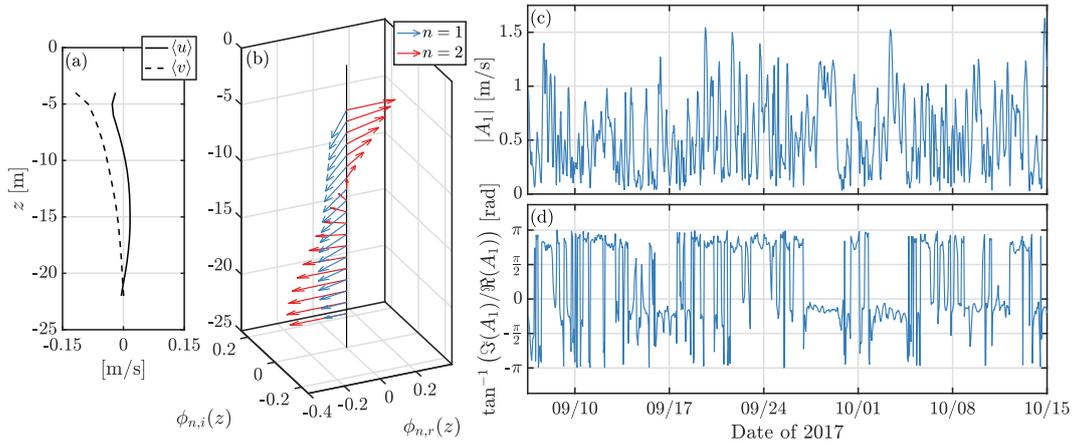


Figure 2. Complex empirical orthogonal function (cEOF) decomposition of (u, v) ADCP velocities at $(x, y) = (-705, -725)$ m: (a) Mean horizontal velocities $(\langle u \rangle, \langle v \rangle)$ as a function of distance below mean sea level z . (b) Structure of cEOFs mode 1 (ϕ_1 , blue) and mode 2 (ϕ_2 , red) versus z , (c) first cEOF $|A_1|$ and (d) phase $(\tan^{-1}[\Im(A_1)/\Re(A_1)])$ time series over the analysis period. Mode 1 and mode 2 capture 52% and 21% of velocity variance, respectively.

226 To further reduce aliasing of short length-scale velocity variability that potentially
 227 alias vorticity, the 2-h low-pass filtered ADCP velocities are additionally smoothed by
 228 reconstructing velocities from a complex empirical orthogonal function (cEOF) decom-
 229 position (*e.g.*, Kundu & Allen, 1976; Kumar et al., 2015). At each moored ADCP, the
 230 2-h low-pass filtered velocities are decomposed into time-mean $(\langle u \rangle, \langle v \rangle)$, where $\langle \rangle$ denotes
 231 a time average over the analysis period) and fluctuating (u', v') components (*i.e.*, $u =$
 232 $\langle u \rangle + u'$). The cEOF decomposition is performed on the complex fluctuating velocity,

$$\psi(z, t) = u'(z, t) + i v'(z, t), \quad (1)$$

233 where $i = \sqrt{-1}$. The complex velocity ψ is decomposed into a set of orthogonal modes

$$\psi(z, t) = \sum_{n=1}^N \phi_n(z) A_n(t), \quad (2)$$

234 where $\phi_n(z)$ is the n -th eigenvector (EOF) of the Hermitian covariance matrix of ψ and
 235 $A_n(t)$ is the amplitude time series of mode n . Both $\phi_n(z)$ and $A_n(t)$ are complex-valued
 236 variables consisting of information related to both $u'(z, t)$ and $v'(z, t)$.

237 An example cEOF decomposition on a 600 kHz Nortek Aquadopp ADCP located
 238 south-west of Pt. Sal at $(x, y) = (-705, -725)$ m and mean depth $h = 25$ m is shown
 239 in Figure 2. The northward time-averaged current $\langle v \rangle$ is negative (southward) and sur-
 240 face intensified near 0.12 m s^{-1} and approximately zero near the bed (Fig. 2a, solid). The
 241 eastward time-averaged current $\langle u \rangle$ is weak ($\approx 0.03 \text{ m s}^{-1}$) and offshore (onshore) in the
 242 upper (lower) water column (Fig 2b, dashed). The cEOF mode $n = 1$ velocity struc-
 243 ture explains 52% of the variance and is mostly barotropic (unidirectional and weakly
 244 depth varying) with near-surface velocities veering roughly 45° counterclockwise (blue,
 245 Fig. 2b). Time-series analysis indicates that the mode $n = 1$ amplitude magnitude
 246 $|A_1|$ is dominated by subtidal and tidal band variability as seen in Fig. 2c. The $A_1(t)$
 247 phase varies bimodally indicating primarily NW to SE flow. The cEOF mode $n = 2$
 248 explains 21% of the variance and has vertical structure that changes sign mid-depth, qual-
 249 itatively consistent with the first baroclinic mode (red, Fig. 2b). Time-series analysis re-
 250 veals that the mode $n = 2$ amplitude A_2 (not shown) has more high-frequency vari-
 251 ability equally split between super-tidal (> 2.2 cpd) and lower-frequencies (< 2.2 cpd).
 252 For cEOF modes $n \geq 3$ (not shown), the variance percentage captured diminishes quickly,
 253 the modes are comprised of high vertical wavenumber variability, and the correspond-
 254 ing amplitudes are dominated by supertidal > 2.2 cpd variability.

255 This cEOF decomposition framework is applied to the ADCPs deployed near Pt. Sal.
 256 At each of these ADCPs, a smoothed velocity is reconstructed using only the first two
 257 cEOF modes, *e.g.*,

$$u(z, t) = \langle u \rangle + \Re \left[\sum_{n=1}^2 \phi_n(z) A_n(t) \right] \quad (3a)$$

$$v(z, t) = \langle v \rangle + \Im \left[\sum_{n=1}^2 \phi_n(z) A_n(t) \right] \quad (3b)$$

258 where \Re and \Im indicate the real and imaginary components, respectively. This recon-
 259 structed velocity captures $73\% \pm 5\%$ of the variance at the 9 ADCPs presented in Fig. 4.
 260 Hereafter, $u(z, t)$ and $v(z, t)$ represent the 2-h low-pass filtered and cEOF (3) reconstructed
 261 ADCP velocities and will be used in subsequent analysis. Excluding higher cEOF modes
 262 removes high frequency (higher horizontal wavenumber) and high vertical wavenumber
 263 noise, giving a smoothed velocity signal for estimating vorticity.

264 At each ADCP, depth-averaged velocities (denoted with capitals, *i.e.*, $[U(t), V(t)]$)
 265 are calculated by vertically averaging ($u(z, t), v(z, t)$) velocity over the vertical range of
 266 valid observations for the entire analysis period. For example, the vertical range for the
 267 ADCP in Fig. 2 is $z = -21$ m to $z = -4$ m. No extrapolation to the free surface or
 268 the bed is performed as it relies on assumptions regarding the surface and bottom bound-
 269 ary layer which may bias the depth-average. Depth-averaged velocity variance major
 270 and minor axis and orientation are calculated (*e.g.*, Emery & Thomson, 2001) from an
 271 eigenvalue decomposition of the (U, V) velocity variance and covariances (*e.g.* $\langle U'^2 \rangle$, $\langle U'V' \rangle$)
 272 yielding principal axis angle θ_p , major axis U_{maj}^2 and minor axis U_{min}^2 variances, allow-
 273 ing for plotting of velocity standard deviation ellipses (analogous to tidal ellipses). The

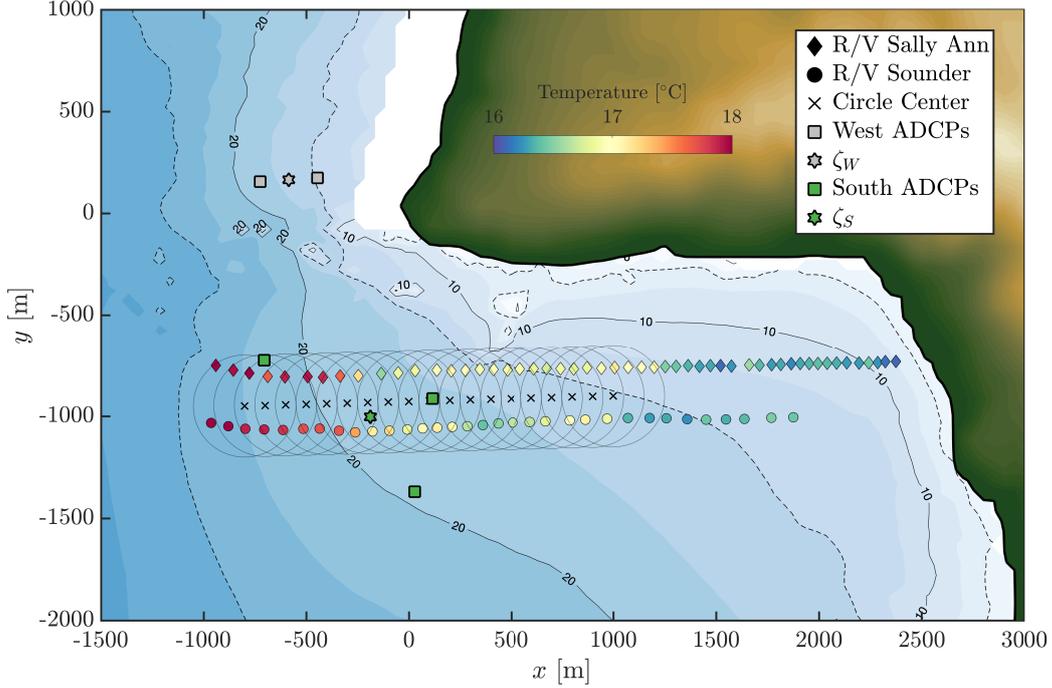


Figure 3. Map of mooring- and vessel-based vorticity estimation locations near Pt. Sal as a function of x and y with local bathymetry. West vorticity ζ_W (gray star) is estimated from west ADCPs (gray squares). South vorticity ζ_S (green star) is estimated at centroid of south ADCP triangle (green squares). For reference, a pair of simultaneous parallel vessel tracks for the *R/V Sally Ann* (colored diamonds) and *R/V Souder* (colored circles) are shown. Colors represent vessel transect near-surface temperature ($z = -1.5$ m) from CTD observations. Data shown are from September 13, 2017, 10:54–11:19 PDT (later denoted as transect 3) and are representative of all transects. For each vessel transect, vessel-based vorticity is estimated at black “x”s (100 m separation) using vessel ADCP observations within the 250 m radius circles (gray).

274 variances (e.g. $\langle U'^2 \rangle$) include variability over subtidal, tidal, and supertidal frequency
 275 bands. Velocity and vorticity variables are decomposed using the PL64 filter (Limeburner
 276 et al., 1985) into subtidal (< 0.73 cpd), diurnal (0.73–1.5 cpd), semi-diurnal (1.5–2.2 cpd)
 277 and supertidal (2.4 cpd to 12 cpd) frequency band components. Statistics (means and
 278 standard deviations) are calculated for each of these frequency band components.

279 **2.2.2 Fixed ADCP vorticity estimation**

280 Estimating ocean vertical vorticity $\zeta = v_x - u_y$ is inherently difficult as two-dimensional
 281 spatial differences of noisy velocity observations are required. Vorticity has been esti-
 282 mated via many methods, including drifters (e.g., Pawlak et al., 2003; Ohlmann et al.,
 283 2017; Spydell et al., 2019), radar (e.g., Kirincich, 2016), gliders (e.g., Zeiden et al., 2019),
 284 and vessels transects (e.g., Geyer & Signell, 1990; Rudnick, 2001; Pawlak et al., 2003;
 285 Shcherbina et al., 2013b; MacKinnon et al., 2019). To reduce noise in the estimated spa-
 286 tial velocity derivatives from fixed-ADCPs motivates the use of the 2-h filtered and cEOF
 287 reconstructed ADCP velocity time-series. Using the moored ADCP velocities (3), ver-

288 tical vorticity ζ is estimated at two locations near Pt. Sal (Fig. 3, green and gray stars).
 289 Vorticity at the “south” location $\zeta_S(z, t)$ ($[x, y] = [-187, -1003]$ m), is estimated with
 290 three ADCPs in a triangular configuration (green squares in Fig. 3) via plane fit to the
 291 2-h low pass and cEOF reconstructed moored ADCP (u, v) velocities. Specifically, (u, v)
 292 are fit to the functions

$$u_i(z, t) = u_S + \frac{\partial u}{\partial x}(x_i - x_S) + \frac{\partial u}{\partial y}(y_i - y_S), \quad (4a)$$

$$v_i(z, t) = v_S + \frac{\partial v}{\partial x}(x_i - x_S) + \frac{\partial v}{\partial y}(y_i - y_S), \quad (4b)$$

293 where i represents the ADCP number, (x_S, y_S) is the centroid of the “south” triangle,
 294 (u_S, v_S) are centroid fit velocities, $\partial(u, v)/\partial x$ and $\partial(u, v)/\partial y$ are the fit velocity gradi-
 295 ents (*e.g.*, Molinari & Kirwan, 1975). The base and height of the triangle (or its edges)
 296 are 464 m and 842 m. This fit is performed for the vertical levels $z = -18$ m to $z =$
 297 -4 m which are present at all 3 ADCPs. This plane fitting method assumes (u, v) vary
 298 linearly in both x and y between the mooring locations. With three ADCPs, the fit is
 299 exact and any ADCP noise or small-scale (u, v) variability will alias noise into the es-
 300 timated velocity gradient. The use of the 2-h low pass filtering and the cEOF velocity
 301 reconstruction reduces the ADCP noise and small-scale spatial (u, v) variability, result-
 302 ing in reduced estimated velocity gradient noise. The velocity gradients calculated from
 303 plane fitting should be interpreted as being constrained to scales on the order of the ADCP
 304 separation (≈ 1 km) and longer, as shorter scale vorticity variability is not resolved. From
 305 the resulting fit parameters, “south” vorticity at the centroid location (green star, Fig. 3)
 306 is estimated as

$$\zeta_S(z, t) = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}. \quad (5)$$

307 At the location just west of Pt. Sal, “west” vorticity $\zeta_W(z, t)$ ($[x, y] = [-585, 165]$ m)
 308 is estimated from two ADCPs in a line extending west off of the point (Fig. 3, gray star
 309 and squares). With only two locations, the plane fit method (5) cannot be used and only
 310 a single vorticity component is estimated analogous to single underway ADCP transects
 311 (*e.g.*, Rudnick, 2001; Zeiden et al., 2019). Here, the 2-h low-pass filtered and cEOF re-
 312 constructed velocities are rotated into an “alongshore” coordinate system (\tilde{u}, \tilde{v}) that is
 313 4.91° east of north, an average of the two ADCP principal axes (Fig. 4). At every 1 m
 314 from $z = -15$ to -4 m where both moorings always had valid data, “west” vorticity
 315 $\zeta_W(z, t)$ is estimated as the cross-shore gradient ($\Delta\tilde{x} = 276$ m) of rotated alongshore
 316 velocity between the two moorings (*i.e.*, $\partial\tilde{v}/\partial\tilde{x}$), neglecting the $\partial\tilde{u}/\partial\tilde{y}$ term. This as-
 317 sumption is likely reasonable as the upstream velocity is locally alongshore uniform (*i.e.*, $\partial\tilde{u}/\partial\tilde{y} \approx$
 318 0). This also assumes that alongshore velocity varies linearly with \tilde{x} constraining the scale
 319 of vorticity to the ≈ 300 m ADCP separation scale. However, for northward flow, $\partial\tilde{u}/\partial\tilde{y}$
 320 could be significant due to flow separation and recirculation west and north of Pt. Sal,
 321 resulting in an incomplete ζ_W estimate. For analysis purposes, the west vorticity ζ_W es-
 322 timate is used for both southward and northward flow conditions. The potential bias in
 323 ζ_W for southward and northward flow is discussed in Appendix A.

324 In addition to vorticity, the centroid velocities at the south (*i.e.*, (u_S, v_S) in Eq. 4)
 325 and west (u_W, v_W) locations are depth averaged over the z -range where the ADCPs used
 326 in the fit had valid data and rotated into their principal axes directions (44.3° west of
 327 north and 4.9° east of north). These principal axes are nearly the average of the indi-
 328 vidual moored ADCP principal axes (Figure 4). The depth-averaged principal axes along-
 329 shore velocities are denoted as V_S and V_W , respectively, and will be used in subsequent
 330 analysis.

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2.3 Vessel-based observations and vorticity estimates

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Here, coordinated vessel-based parallel transects from SIO’s *R/V Sally Ann* and UW-APL’s *R/V Sounder* from IOP1 on 13 September were used to estimate both vorticity components as in Shcherbina et al. (2013b). Both vessels performed tow-yo CTD casts using RBR Concerto CTDs sampling at 6 Hz (*Sally Ann*) or 12 Hz (*Sounder*) with an accuracy of 0.002°C . Data from each cast are filtered with half-power cutoff of 0.25 m and vertically gridded to 0.1 m resolution. Each vessel also was equipped with a pole-mounted, downward-looking TeleDyne RDI WorkHorse ADCP capable of bottom tracking. *R/V Sally Ann* had a RDI 300 kHz ADCP with 1 m vertical bins and 1 s sampling intervals while *R/V Sounder* had a RDI 1200 kHz ADCP with 1 m bins and 3 s sampling intervals. Note the 18 m profiling range is within the RDI 1200 kHz ADCP manufacturer’s upper limit. ADCP data for both vessels were averaged down to 1 minute. During transects the *R/V Sally Ann* and *R/V Sounder* vessel speeds were approximately 1 m s^{-1} and 1.7 m s^{-1} , respectively. This yielded average ADCP spatial resolution of 62 m and 102 m, respectively and average CTD cast spatial resolution of 65 m and 89 m, respectively.

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On 13 September, three repeated west to east parallel transects were conducted south of Pt. Sal by *R/Vs Sally Ann* and *Sounder*, intersecting the triangle used to calculate ζ_S (Figure 3). These parallel transects occurred during southward flow in the lee of Pt. Sal and were north-south separated by approximately 250–300 m (Figure 3). The 10:54–11:19 PDT transect provides an example of the surface temperature structure in the lee of Pt. Sal. Near-surface temperature varied from warm (near 18°C) farther offshore to cold (near 16°C) within the bay on both transects (Figure 3). A $\Delta T \approx 1^{\circ}\text{C}$ temperature front is evident between $-500 < x < 0$ m, near the south vorticity centroid location (green star in Figure 3). Vessel-based temperature transects are estimated by averaging CTD temperature between the *R/V Sally Ann* and *Sounder*. If one vessel is missing data, the average is not calculated. As CTD casts were not full water-column depth, temperature is estimated over the upper 2/3 of the water column.

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Vessel-based vorticity $\zeta_V(x, z)$ is calculated at the center of the two parallel transects from $-1000 \leq x \leq 1000$ m at 100 m intervals (see “x” in Figure 3) At each “x” location, all vessel-based (u, v) data that fall within a search circle of radius $R = 250$ m are used to least-squares plane-fit velocity gradients (*i.e.*, Eq. 4) at particular z levels. Velocity gradients are estimated from $-20.5 \leq z \leq -2.5$ m at 1 m intervals. Best-fits are removed when circles have fewer than 5 data points or when observations are time-separated by more than 15 min, to minimize aliasing from temporal and spatial misalignment in vessel sampling. Vorticity at each “x” is then estimated from the best-fit velocity gradients, which then provides a spatial map of $\zeta_V(x, z)$ for each transect. This process is repeated for the three parallel transects conducted on this day.

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3 Spatial structure and temporal variability of vorticity estimates

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3.1 Fixed-location depth-averaged velocity statistics near Pt. Sal

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Before examining vorticity, we first examine the depth-averaged (barotropic) velocity statistics within a few km of Pt. Sal (Figure 4) to provide context about the barotropic flow around the headland. Depth-averaged velocity means and standard deviation ellipses (analogous to tidal ellipses) are calculated over the analysis period (13:00PDT 6-Sept to 06:00PDT 15-Oct) and standard deviations include variability over subtidal, tidal, and supertidal frequency bands. For $y > 0$ m (west and north of Pt. Sal), the time-

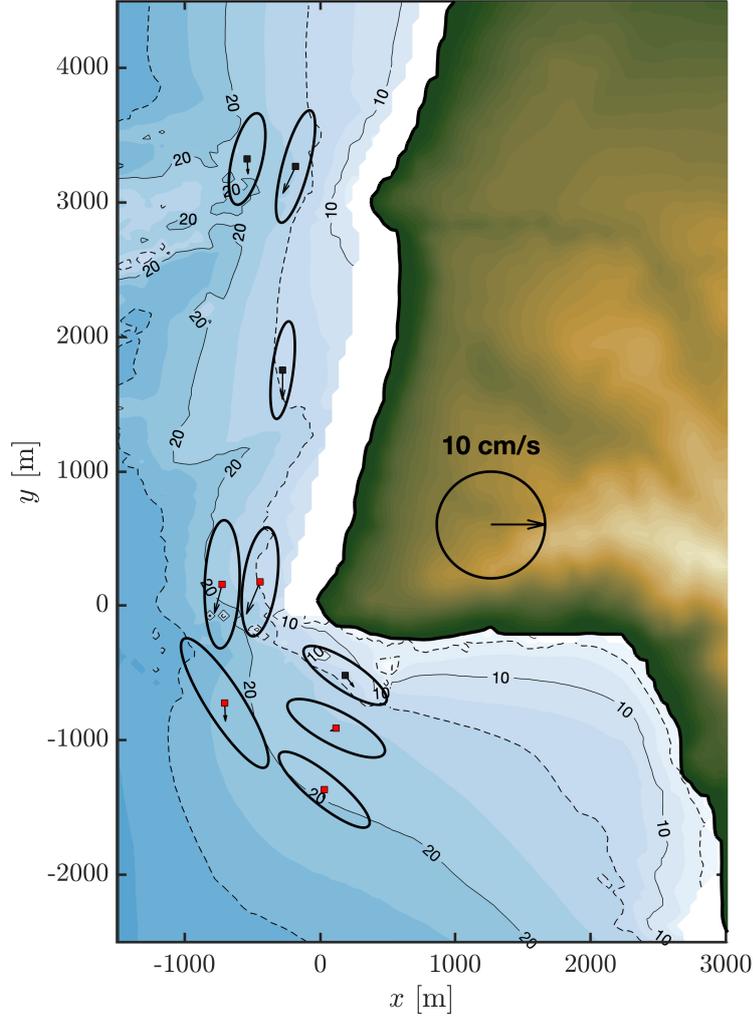


Figure 4. Fixed-location ADCP depth-averaged velocity time-means (arrow) and standard deviation ellipses (black ellipse) as a function of x and y near Pt. Sal. Ellipses have major and minor axes as U_{maj} and U_{min} and orientation angle θ_p , and are analogous to tidal ellipses but include all frequency bands. Time-averaging is over the analysis period (13:00PDT 6-Sept to 06:00PDT 15-Oct). Solid contours are 10 and 20 m isobaths with dashed contours denoting 5 m intervals. White denotes regions without bathymetry data.

377 mean (over the analysis period) and depth-averaged velocities are largely southward and
 378 along-isobath with magnitudes of $0.03\text{--}0.05\text{ m s}^{-1}$ (arrows in Figure 4). For $y < 0\text{ m}$
 379 (south of Pt. Sal), the time-mean depth-averaged velocities are weaker ($0.01\text{--}0.02\text{ m s}^{-1}$)
 380 with variable directions. Over all ADCPs the principal (major) axis velocity standard
 381 deviation (*i.e.*, U_{maj}) varies between $0.09\text{--}0.14\text{ m s}^{-1}$ (ellipses in Figure 4), substantially
 382 larger than the mean flow, and is largely oriented along-isobath. Depth-averaged cur-
 383 rent variability is strongly polarized with minor to major axis standard deviation $U_{\text{min}}/U_{\text{maj}}$
 384 between $0.2\text{--}0.3$. The depth-averaged current variability is roughly comprised of equal
 385 subtidal and tidal (diurnal and semidiurnal) variability.

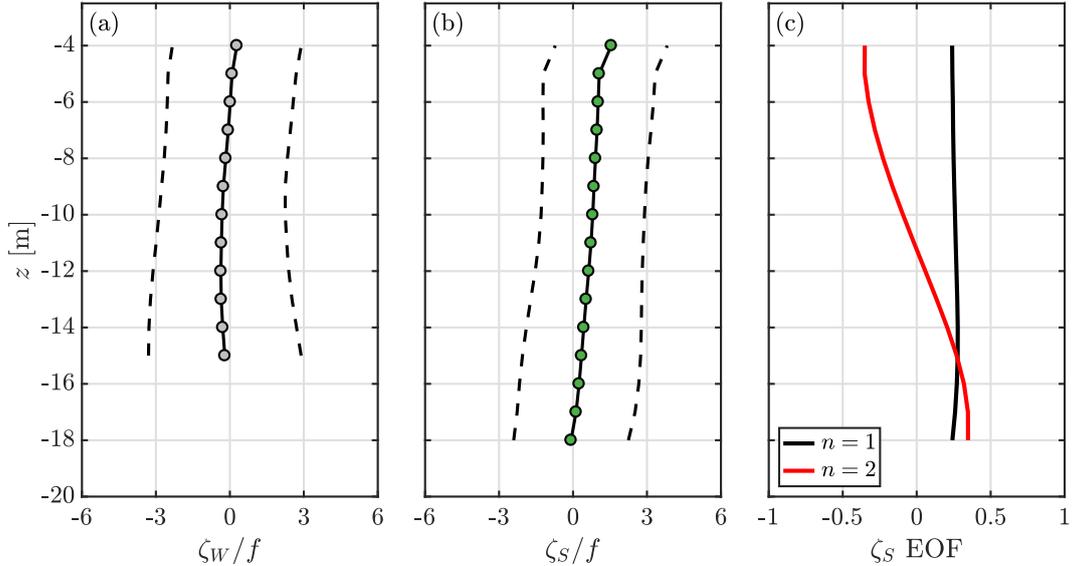


Figure 5. Time-mean (solid) and standard deviation (dashed) of normalized vorticity ζ/f versus depth z at the (a) west ζ_W and (b) south ζ_S locations (Figure 3). (c) South vorticity ζ_S EOF modes 1 and 2 versus z , representing 64% and 27% of variability, respectively. Statistics are calculated over the analysis period (13:00PDT 6-Sept to 06:00PDT 15-Oct).

386 The relative orientation of the velocity standard deviation ellipses reveals aspects
 387 relevant to vorticity (Figure 4). For example, near the small headland (Mussel Rock, $y \approx$
 388 3000 m), southward flow velocities are generally stronger closer to shore likely due to the
 389 very rough bathymetry (denoted rocky outcrop in Colosi et al., 2018) enhancing drag
 390 near the offshore ADCP. In contrast, just west of Pt. Sal (red squares west of Pt. Sal,
 391 Figure 4), southward flow velocities are generally weaker in shallower water. South of
 392 Pt. Sal, velocity ellipses rotate to the southeast quasi-following bathymetry contours. The
 393 ADCPs used for south vorticity (ζ_S) all have different ellipse orientations demonstrat-
 394 ing presence of non-zero depth-averaged vorticity.

395 3.2 Fixed-location vorticity

396 Here, we examine the vertical structure of the two fixed-location vorticity estimates
 397 (ζ_W and ζ_S) and subsequently the time-variability of the depth-averaged vorticity in the
 398 context of barotropic tide and depth-averaged along-headland velocity. The time means
 399 and standard deviations (over the analysis period, 13:00PDT 6-Sept to 06:00PDT 15-
 400 Oct) of ζ_W and ζ_S vertical structure are shown in (Figure 5a,b). For all analyses, vor-
 401 ticity is normalized by the local inertial frequency $f = 8.34 \times 10^{-5} \text{ s}^{-1}$. At the west-
 402 ern location (Figure 5a), time-mean vorticity $\langle \zeta_W \rangle / f$ is near zero throughout the wa-
 403 ter column with largely vertically uniform standard deviations of approximately ± 3 . At
 404 the southern location (Figure 5b), mean vorticity $\langle \zeta_S \rangle / f$ increases with z , from near-zero
 405 close to the bed to $1.6f$ near-surface. The ζ_S standard deviation (std) is slightly weaker
 406 near ≈ 2.25 and slightly more depth uniform than ζ_W . Note, the west location vortic-
 407 ity statistics are potentially biased for northward flow (Appendix A).

408 Although the vertical structure of vorticity variability is largely depth uniform (Fig-
 409 ure 5a,b), the vertical coherence of said variability is examined with a vertical EOF de-

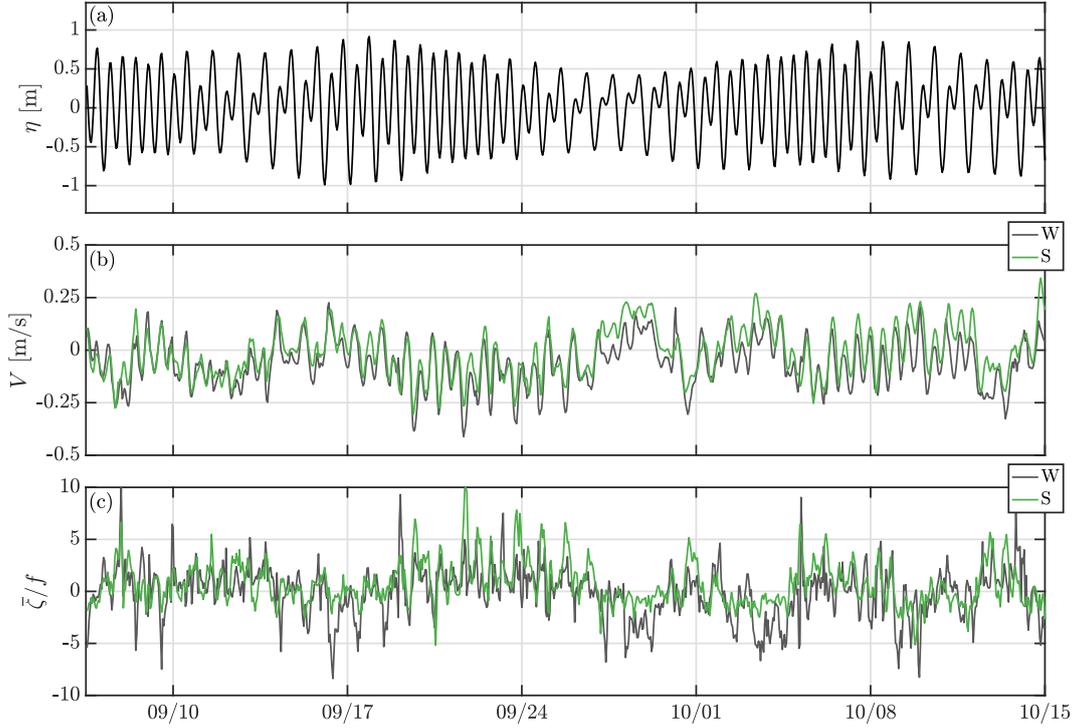


Figure 6. Time-series of (a) tidal elevation η , (b) depth-averaged centroid principal axes alongshore velocity V , and (c) normalized depth-averaged vorticity $\bar{\zeta}/f$. In (b,c), gray and green correspond to west and south locations, respectively. In panels (b,c), The correlation between V_S and V_W is $r = 0.86$ and between $\bar{\zeta}_S/f$ and $\bar{\zeta}_W/f$ is $r = 0.55$.

410 composition on both ζ_S and ζ_W . The 1st EOF mode for ζ_S (black line) is strongly barotropic
 411 and captures 64% of the vorticity variance whereas the 2nd EOF mode (red line) has a
 412 mode-1 baroclinic structure accounting for 27% of variance (Figure 5c). Both EOF modes
 413 1 and 2 for ζ_W are similar to those for ζ_S in both vertical structure (not shown) and vari-
 414 ance fraction (65% and 27%, respectively). The vertically smooth ζ/f means and low
 415 mode dominance of ζ/f variability indicates that the vorticity estimation method using
 416 2-h filtered and cEOF reconstructed velocities (Section 2.2.1) is not noise contam-
 417 inated due to aliasing of short scale variability associated with internal warm bores or
 418 solitons (Colosi et al., 2018; McSweeney et al., 2020) that likely have contributions at
 419 cEOF mode 2. If noise were significant, one would expect small-scale vertical variation
 420 in the statistics due to estimation error. That the temporal ζ variability is largely depth-
 421 uniform also indicates that the depth-averaged vorticity can be used to study the vorticity
 422 kinematics and dynamics. Here, the depth-averaged vorticity is denoted with an overbar
 423 (*i.e.*, $\bar{\zeta}_S$) and as with depth-averaged V is the average over the vertical range
 424 where vorticity could be estimated. Subsequent analyses are conducted with depth-averaged,
 425 normalized vorticity $\bar{\zeta}/f$.

426 The time-series of tidal elevation η , depth-averaged centroid principal-axes along-
 427 shore velocity (V_S, V_W), and depth-averaged vorticity ($\bar{\zeta}_S/f, \bar{\zeta}_W/f$) are used to to exam-
 428 ine the time-scales of variability of each and the similarities, and differences between the
 429 west and south locations. Recall, that velocity and vorticity variables are decomposed
 430 into subtidal, diurnal, semidiurnal, and supertidal components from which statistics are

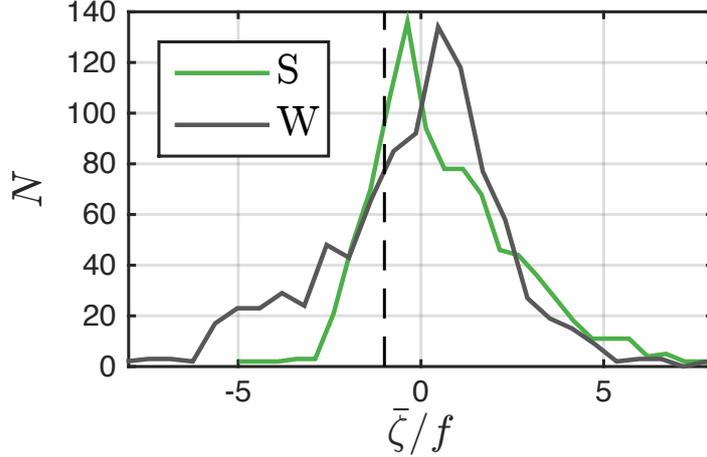


Figure 7. Histogram of south $\bar{\zeta}_S/f$ (green) and west $\bar{\zeta}_W/f$ (gray) normalized vorticity. The vertical dashed line represents $\bar{\zeta}/f = -1$ or zero potential vorticity. The vorticity $\bar{\zeta}_S/f$ skewness is 0.88, significantly elevated over $\bar{\zeta}_W/f$ skewness of -0.19. Note that $\bar{\zeta}_S/f < -1$ and $\bar{\zeta}_W/f < -1$ (*i.e.*, left of the dashed line) for 19% and 31% of the time, respectively.

431 calculated (Section 2.2.1). The analysis period (13:00PDT 6-Sept to 06:00PDT 15-Oct)
 432 spanned nearly 3 spring-neap tidal cycles (Figure 6a), with spring tides of ± 1 m and neap
 433 tides of ± 0.5 m. The depth-averaged V_S and V_W vary largely from ± 0.2 m s^{-1} with (semid-
 434 iurnal and diurnal) tidal and subtidal variability (Figure 6b). At the west location, the
 435 time mean flow is southward ($\langle V_W \rangle = -0.06$ m s^{-1}), but near-zero at the south loca-
 436 tion ($\langle V_S \rangle = 0.01$ m s^{-1}). The V_S and V_W have similar std (≈ 0.12 m s^{-1}) and are well
 437 correlated ($r = 0.86$) across the tidal and subtidal time-scales. At the south location,
 438 subtidal variability is dominant with velocity amplitude (not std) of 0.13 m s^{-1} . Semid-
 439 iurnal variability is second largest with spring neap velocity amplitude varies from 0.03 –
 440 0.1 m s^{-1} . The west location is similar. The depth-averaged $\bar{\zeta}_S/f$ and $\bar{\zeta}_W/f$ vary ± 8 with
 441 subtidal, tidal, and more high-frequency variability than V (Figure 6c). The time mean
 442 south vorticity $\langle \bar{\zeta}_S/f \rangle = 0.7$ is elevated relative to the west vorticity $\langle \bar{\zeta}_W/f \rangle = 0.2$.
 443 In contrast, the west location $\text{std}(\bar{\zeta}_W/f) = 2.5$ is elevated compared to $\text{std}(\bar{\zeta}_S/f) =$
 444 2.1 , consistent with the vorticity standard deviations over the vertical (Figure 5a,b). Rel-
 445 ative to velocity, the elevated high frequency vorticity variability is expected as the higher
 446 horizontal wavenumbers of vorticity correspond to higher frequencies in steady and os-
 447 cillatory flows (Lumley & Terray, 1983b). The west and south vorticity is less correlated
 448 ($r = 0.55$) than for V , which may be due to vorticity generation between the two loca-
 449 tions or west-location vorticity bias (Appendix A).

450 Histograms of south ($\bar{\zeta}_S/f$) and west ($\bar{\zeta}_W/f$) vorticity reveal differences between
 451 the two locations (Figure 7). The $\bar{\zeta}_S/f$ distribution is highly skewed around the mean
 452 $\langle \bar{\zeta}_S/f \rangle = 0.7$, with much higher probability of large positive than negative $\bar{\zeta}_S/f$ (green
 453 curve in Figure 7). The skewness $\langle (\bar{\zeta}_S/f)^3 \rangle / \langle (\bar{\zeta}_S/f)^2 \rangle^{3/2} = 0.88$ is strongly positive
 454 and only infrequently (19%) is the south location potential vorticity negative (*i.e.*, $\bar{\zeta}_S/f <$
 455 -1 , left of dashed line in Figure 7). Such strong positive skewness is qualitatively consis-
 456 tent with Gulf Stream vorticity observations on similar spatial scales (Shcherbina et
 457 al., 2013a). In contrast, the $\bar{\zeta}_W/f$ distribution (gray curve in Figure 7) is much more
 458 symmetric around mean $\langle \bar{\zeta}_W/f \rangle = 0.2$, with smaller and opposite signed skewness of

459 -0.19 . The west location potential vorticity is negative ($\bar{\zeta}_W/f < -1$) 31% of the time,
 460 much more frequently than for $\bar{\zeta}_S/f$. Velocity skewness at V_S is 0.22 and for V_W is -0.11 ,
 461 much less pronounced than vorticity skewness but with similar signs. The differences in
 462 the vorticity distributions are also evident in the time-series (Figure 6c). Away from
 463 boundaries and surface or bottom forcing, strong anticyclonic flows ($\bar{\zeta}/f < -1$) are un-
 464 stable (*e.g.*, Hoskins, 1974) and are thus less likely. For example, Shcherbina et al. (2013a)
 465 observe Gulf Stream near-surface $\zeta/f < -1$ about 5% of the time. In contrast, the en-
 466 hanced likelihood of $\bar{\zeta}/f < -1$ at the west (31%) and south (19%) locations indicates
 467 strong vorticity generation effects. This will be examined further in Section 5. As dis-
 468 cussed in Appendix A, northward flow may bias the negative $\bar{\zeta}_W/f$ magnitude low.

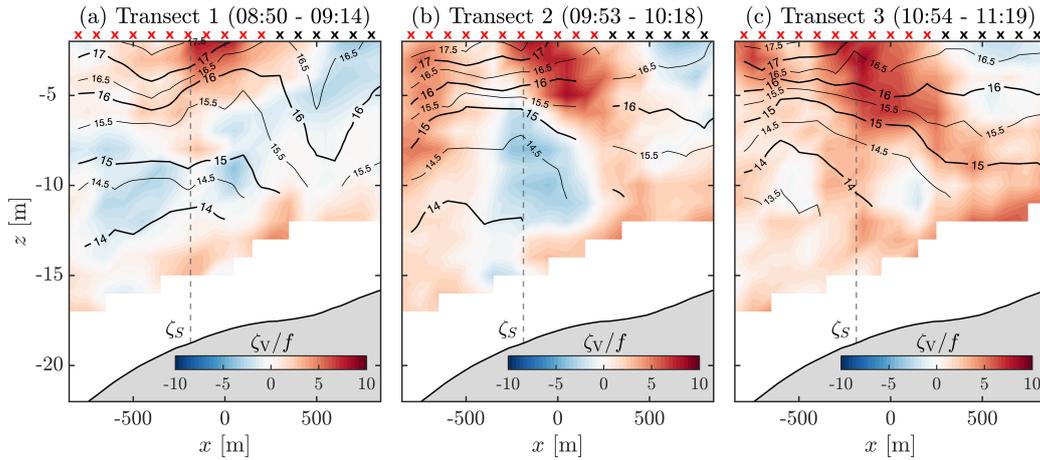


Figure 8. Normalized vessel-based vorticity ζ_V/f (color) sections as a function of x and z with overlaid vessel-averaged averaged temperature T (solid black lines) for transects (a) 1 (08:50-9:14), (b) 2 (09:53-10:18), and (c) 3 (10:54-11:19). The x location of ζ_S is indicated by the vertical dashed line. Bathymetry is shown in gray. The 'x's above each panel represent locations where vorticity is estimated, and red 'x's represent locations within the triangle used to estimate $\bar{\zeta}_S/f$.

469 3.3 Vessel-based vorticity

470 Next, we examine vorticity variability at short time-scales (few hours) and relatively
 471 short length-scales (100–1000 m) using three vessel-based vorticity and temperature tran-
 472 sects (Section 2.3) shown in Figure 8. Recall, these vessel observations are based on 1-
 473 min averages (60–100 m spatial scales) and are essentially snapshots relative to the 2-
 474 h low-pass filtered and cEOF reconstructed fixed ADCP observations. In transect 1 (08:50–
 475 09:14, Figure 8a), near surface ($z > -5$ m) ζ_V/f is largely positive near $+2$ for $x <$
 476 500 m with a 400 m-wide elevated patch $\zeta_V/f \approx 8$ near $x = 0$ m. In an intermediate
 477 layer ($-12 < z < -5$ m), $\zeta_V/f \approx -2$ is largely negative and surface outcrops for $x >$
 478 500 m, associated with near-surface colder water (*e.g.*, Figure 3) and an isotherm trough
 479 at $x \approx 500$ m. In the region for $x < 200$ m, the stratification is relatively weak with
 480 a roughly $\Delta z = 6$ m separation between the 15°C and 17°C isotherms. Near bed ($z <$
 481 -12 m), $\zeta_V/f \approx 2$ is largely positive.

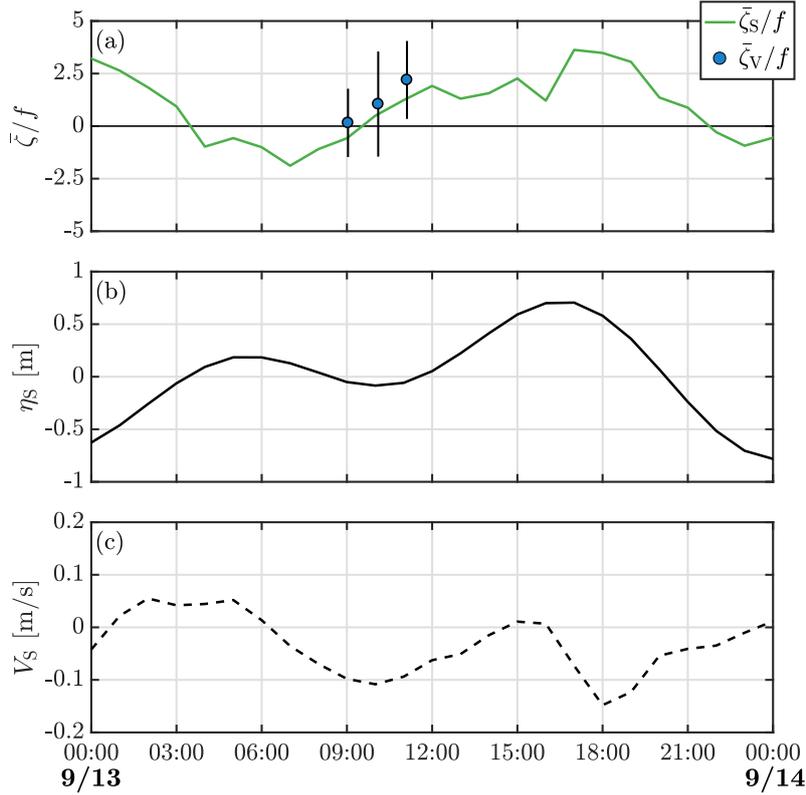


Figure 9. (a) Time-series of 13-Sept south-location hourly depth-averaged vorticity $\bar{\zeta}_S/f$ (green line) and concurrent vessel transect-averaged vorticity $\bar{\zeta}_V/f$ (blue circles). Transect-averaged $\bar{\zeta}_V/f$ is vertically averaged from near-bed to $z = -4.5$ m and cross-shore averaged from $x = -800$ m to 200 m. The blue circle is located at the transect mid-point time and the circle width represents the transect duration. Vertical bars on circles are the standard deviation of ζ_V/f over the averaging region. (b) Hourly tidal elevation η_S (black, solid) and (c) depth-averaged principal axis velocity V_S (black, dashed) 13-Sept time series from the southern vorticity estimate location.

482 With later transects, vorticity mostly increases and the 15°C and 17°C isotherms
 483 tilt downward and upward onshore, respectively (Figure 8b,c). In the near-surface ($z >$
 484 -5 m) of transect 2 (09:53–10:18, Figure 8b), two strong positive ζ_V/f patches are present.
 485 The $x \approx 0$ m patch from transect 1 has become larger with maximum $\zeta_V/f \approx 8$, and
 486 a second patch near $x = -700$ m is evident at $\zeta_V/f \approx 5$. Small negative ζ_V/f is seen
 487 near-surface for $x > 500$ m and subsurface near $x = -200$ m. The isotherm tilting
 488 has increased upper-water column stratification at $x = -500$ m. In transect 3 (10:54–
 489 11:19, 8c), ζ_V/f continues to increase and is positive almost everywhere for $x < 300$ m.
 490 The near-surface $\zeta_V/f \approx 8$ patch at $x \approx 0$ m is much larger, but near-surface weak
 491 negative ζ_V/f persists onshore $x > 500$ m. The tilting of the 15°C and 17°C isotherms
 492 has increased, further increasing the upper-water column stratification near $x = -500$ m.

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3.4 Inter-comparison between fixed- and vessel-based vorticity

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Here, we inter-compare the fixed- ($\bar{\zeta}_S/f$) and vessel-based ($\bar{\zeta}_V/f$) vorticity estimates (Figure 9). For each vessel transect, a mean (depth- and cross-shore averaged) vorticity $\bar{\zeta}_V/f$ is estimated from the transect $\zeta_V(x, z)$ (Figure 8) by vertically averaging from the near-bed to $z = -4.5$ m and cross-shore averaging from $x = -800$ m to $x = 200$ m (indicated with red ‘x’ in Figure 8). The vertical and horizontal averaging ranges are chosen to be consistent with the depth coverage and horizontal scale of the fixed ADCPs used to estimate $\bar{\zeta}_S/f$ (Figure 3). The standard deviation of ζ_V/f is also similarly estimated. The time of the transect-averaged $\bar{\zeta}_V/f$ is the median time of the $x = -800$ to $x = 200$ m portion of the transect. No additional filtering of ζ_V/f is performed, contrasting with the 2-h low-pass filtered and cEOF reconstructed fixed ADCP velocities.

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Over the 24 h of 13 Sept, the fixed $\bar{\zeta}_S/f$ varied quasi-diurnally from roughly -2 to 3 (Figure 9a). The barotropic tide was mixed diurnal and semi-diurnal with about 1.2 m range (Figure 9b). The depth-averaged south velocity V_S was largely negative with semidiurnal fluctuations between -0.1 to 0 m s^{-1} (Figure 9c). During the transect time period (08:50–11:19), $\bar{\zeta}_S/f$ increased quasi linearly from near 0 to 2, as the tide underwent an ebb to flood transition. The time period of the transects corresponded to maximal southward flow $V_S = -0.1$ m s^{-1} with a transition from weak negative to positive acceleration.

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The three discrete vessel vorticity $\bar{\zeta}_V/f$ estimates are similar to $\bar{\zeta}_S/f$ with same increasing vorticity trend and the fixed $\bar{\zeta}_S/f$ are always within < 0.4 standard deviations of $\bar{\zeta}_V/f$ (Figure 9a). This suggests that $\bar{\zeta}_V/f$ is biased high relative to $\bar{\zeta}_S/f$ with average error of ≈ 0.5 , but that otherwise these vorticity estimates are robust. The elevated $\bar{\zeta}_V/f$ bias may be because the vessel vorticity $\zeta_V(x, z)$ is estimated on smaller length-scales (*i.e.*, a search radius of 250 m), whereas $\bar{\zeta}_S/f$ is estimated over a scale of ≈ 1000 m using time- and vertical smoothed velocities (Section 2.2.1). Thus, $\zeta_V(x, z)$ contains more high horizontal wavenumber variability (for example, see the 400 m wide $\zeta_V/f > 5$ patch in Figure 8b). Alternatively, negatively biased $\bar{\zeta}_S/f$ (relative to $\bar{\zeta}_V/f$) may result from weak near bottom vorticity ($-18 < z < -14$ m, Figure 5b), whereas ζ_V is on average estimated only to $z \approx -15$ m (Figure 8). Overall, the $\bar{\zeta}_S/f$ and $\bar{\zeta}_V/f$ similarity indicates robust depth-averaged vorticity estimates and provides confidence in subsequent analysis using $\bar{\zeta}_S/f$.

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4 Local Vorticity and Velocity Relationship

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Based on steady flow Rossby number dependence (*e.g.*, Castelao & Barth, 2006; Dong et al., 2007), the near-headland vorticity is expected to be negatively related to the along-headland flow. For time-dependent (reversing) flows, vorticity can also recirculate around a headland (*e.g.*, Signell & Geyer, 1991). Here, we examine the hourly $\bar{\zeta}_S/f$ and $\bar{\zeta}_W/f$ vorticity dependence on the local major-axis depth-average velocity (V_S and V_W) and its time-derivative at both south and west locations (Figure 10). At the south location, $\bar{\zeta}_S/f$ is generally positive for southward flow ($V_S < 0$), and negative for northward flow ($V_S > 0$) with squared correlation $r^2 = 0.42$ (Figure 10a). This negative-signed vorticity-velocity relationship is expected in a steady flow paradigm. The binned-mean $\bar{\zeta}_S/f$ and V_S relationship is tighter ($r^2 = 0.94$), and highlights an asymmetry in slope that depends on the V_S sign. For $V_S < 0$ (*i.e.*, $\bar{\zeta}_S/f$ in the lee of Pt. Sal) the resulting $\bar{\zeta}_S/f$ magnitude (*i.e.*, ≈ 3.8 for $V_S = -0.2$ m s^{-1}) is larger than for $V_S > 0$ when located upstream of Pt. Sal (*i.e.*, $\bar{\zeta}_S/f \approx -1.5$ for $V_S = 0.2$ m s^{-1}). This asymmetry is consistent with vorticity generation at the headland or farther upstream. The

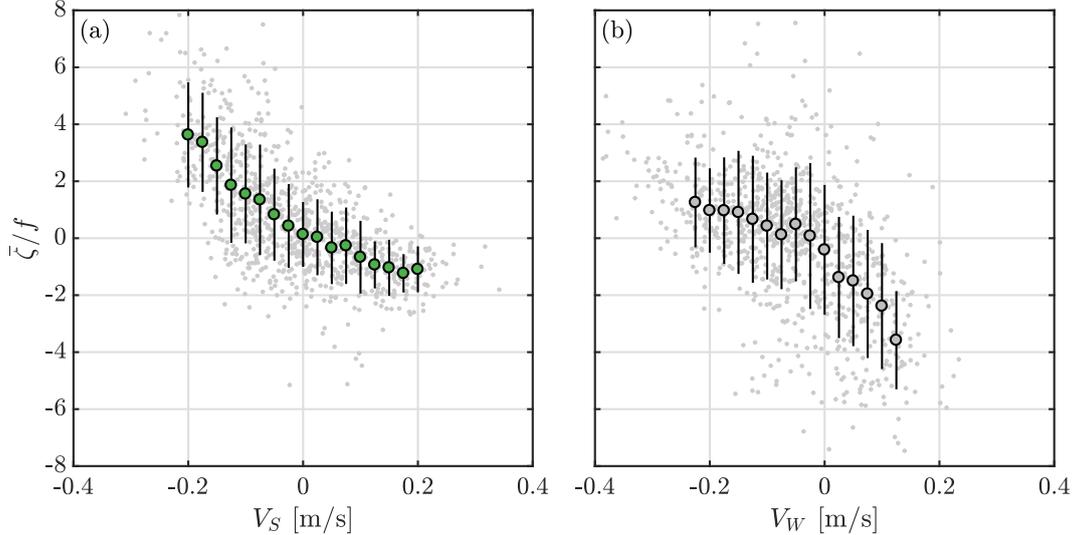


Figure 10. Depth-averaged vorticity versus local depth-averaged principal axis velocity for (a) south location $\bar{\zeta}_S/f$ versus V_S and (b) west location $\bar{\zeta}_W/f$ versus V_W . Light gray dots are hourly data. Green and gray dots are bin-averaged into 2.5 cm s^{-1} bins, with bin standard deviation indicated by vertical black lines. Bins have a minimum of 15 data points.

540 scatter in the hourly data (light gray dots and binned-mean std) range from 0.7–2, sug-
 541 gesting other, non-steady processes are also occurring.

542 At the west location, a similar negative-signed relationship between hourly $\bar{\zeta}_W/f$
 543 and V_W is observed, albeit with lower $r^2 = 0.29$ (Figure 10b). The binned-mean $\bar{\zeta}_W/f$
 544 and V_W squared correlations ($r^2 = 0.88$) is also tighter. A $\bar{\zeta}_W/f$ and V_W slope asym-
 545 metry also is evident that depends on the V_W sign. However, the west location asym-
 546 metry is opposite that of the south location. For both locations at a particular $|V|$, the
 547 $|\bar{\zeta}/f|$ is largest when located in the lee of Pt. Sal. This is again consistent with upstream
 548 or headland vorticity generation. The $\bar{\zeta}/f$ and V slope in the lee is $1.5\times$ stronger for the
 549 west versus the south location (Figure 10), despite the missing $\partial\tilde{u}/\partial\tilde{y}$ in the estimated
 550 $\bar{\zeta}_W/f$ (Section 2.2.2). For $V_W > 0$, the $\bar{\zeta}_W/f$ is likely even more negative (Appendix
 551 A). The $\bar{\zeta}_W/f$ and V_W scatter is larger than at the south location (binned standard de-
 552 viations are larger and range from 1.5–2.6) without a V_W dependence.

553 The $\bar{\zeta}/f$ (non-dimensional) and V (unit m s^{-1}) relationship (Figure 10) is not di-
 554 mensionally consistent, and so cannot be generalized to other headlands. However, the
 555 $\bar{\zeta}/f$ and V relationship can help understand the length-scales of the headland wake vor-
 556 ticity. For example, $V_S = -0.2 \text{ m s}^{-1}$ on average corresponds to $\bar{\zeta}_S/f = 3.8$. With a
 557 vorticity scaling as V/L_v this implies a wake vorticity length-scale of $L_v = 630 \text{ m}$, qual-
 558 itatively consistent with Figure 1 and the assumed $L \sim 1 \text{ km}$ headland scale. At the
 559 west location, binned-mean $\bar{\zeta}_W/f = 3.5$ for $V_W = -0.12 \text{ m s}^{-1}$, resulting in a some-
 560 what shorter length-scale $L_v = 410 \text{ m}$. Where Pt. Sal sits in non-dimensional param-
 561 eter space will be explored in the Discussion.

562 At the south and west locations, the bin-averaged $\bar{\zeta}/f$ and V relationship (Figure 10)
 563 indicates a consistency with steady flow concepts as well as headland or farther upstream
 564 vorticity generation. However, the scatter in the relationship suggests that the time-varying
 565 (oscillatory) nature of the flow may also play an important role in vorticity evolution.

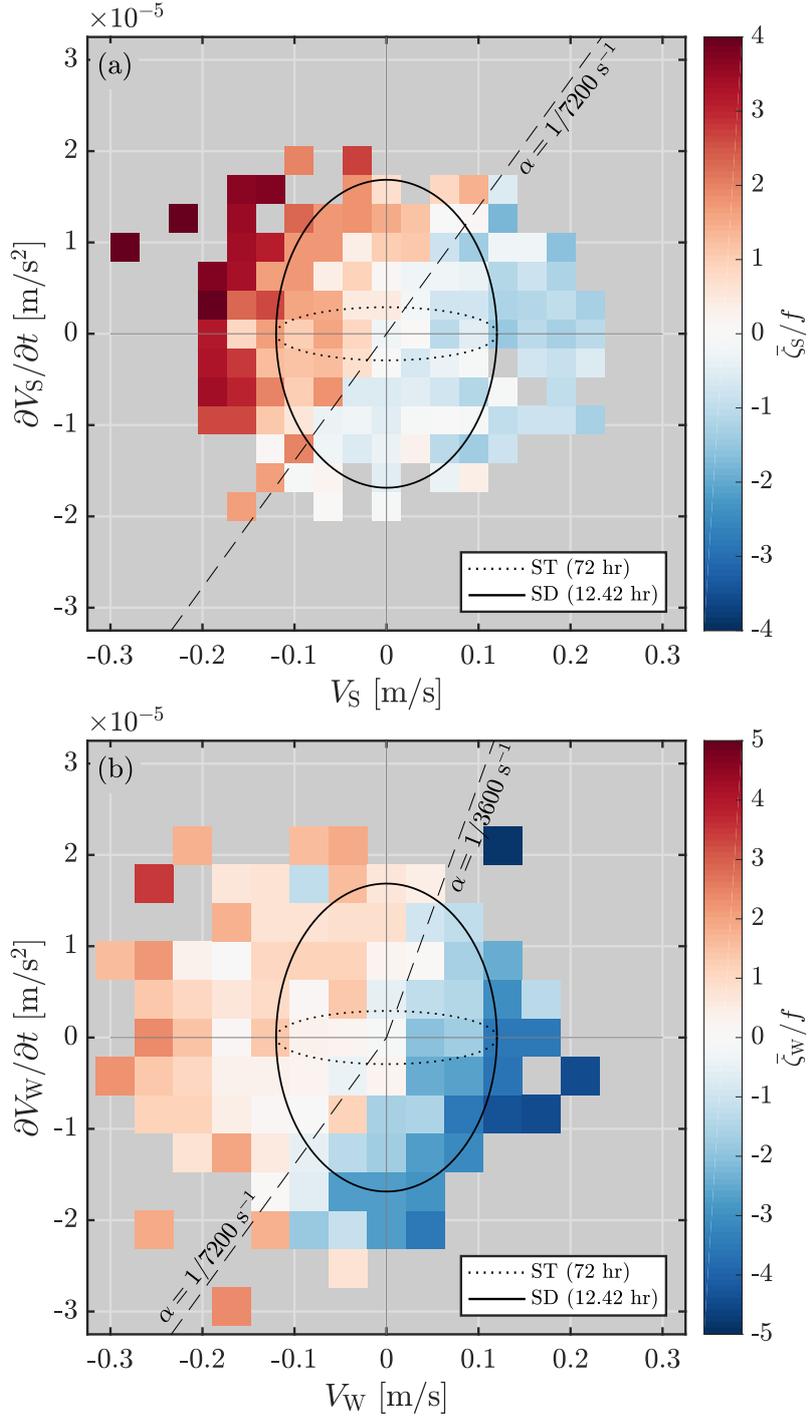


Figure 11. Bin-mean $\bar{\zeta}/f$ (colored) as a function of the depth-averaged principal axis velocity V and acceleration $\partial V/\partial t$ at (a) south location and (b) west location. Bins with fewer than three data points are removed. In (a) dashed line shows a zero-vorticity slope (6) of $\alpha = 1/7200 \text{ s}^{-1}$ and in (b) the dashed line has $\alpha = 1/3600 \text{ s}^{-1}$ and $\alpha = 1/7200 \text{ s}^{-1}$ in the upper-right and lower-left quadrants, respectively. In (a,b), the solid and dotted ellipses show the clockwise orbital paths in V_S and $\partial V_S/\partial t$ phase space of a semi-diurnal (SD, 12.42 h period) and subtidal (ST, 72 h period) periodic flow (11) with amplitude of 0.12 m s^{-1} .

566 At both south and west locations, the binned-mean $\bar{\zeta}/f$ depends strongly on both V and
 567 local acceleration $\partial V/\partial t$ (Figure 11). Note that time-varying flow moves clockwise in V
 568 and $\partial V/\partial t$ phase space in Figure 11 and has to cross $\partial V/\partial t = 0$ for V to have an ex-
 569 tremum. Considering first the south location and times of weak acceleration $\partial V_S/\partial t \approx$
 570 0 , binned-averaged $\bar{\zeta}_S/f$ is related to $-V_S$, consistent with Figure 10a. In a pure steady
 571 flow paradigm, $V_S \approx 0$ should give $\bar{\zeta}_S/f \approx 0$. However, for $V_S \approx 0$, binned-averaged
 572 $\bar{\zeta}_S/f$ is largely proportional to $\partial V_S/\partial t$. For example, with $V_S \approx 0$, $\bar{\zeta}_S/f \approx 2$ for posi-
 573 tive $\partial V_S/\partial t = 1.5 \times 10^{-5} \text{ m s}^{-2}$ indicating that the previously generated positive vorticity
 574 from earlier southward flow ($V_S < 0$) is still present. Moving through phase space,
 575 as V_S becomes positive and as $\partial V_S/\partial t > 0$ continues, $\bar{\zeta}_S/f$ remains positive as previ-
 576 ously generated positive $\bar{\zeta}_S/f$ is advected back northward (upper right quadrant, Fig-
 577 ure 11a), suggesting vorticity is recirculating across the headland. Later, as positive (north-
 578 ward) V_S strengthens and $\partial V_S/\partial t$ weakens, bin-average $\bar{\zeta}_S/f$ undergoes a sign transition
 579 and becomes negative. This $\bar{\zeta}_S/f$ sign transition (*i.e.*, $\bar{\zeta}_S/f = 0$) occurs on the *zero vor-*
 580 *ticity slope*

$$\alpha = \frac{\partial V_S/\partial t}{V_S} \quad (6)$$

581 of $\alpha \approx 1/7200 \text{ s}^{-1}$ (dashed line in Figure 11a) suggesting a vorticity adjustment time-
 582 scale of $\approx 2 \text{ h}$ (Section 6.1). As V_S goes from positive to negative and $\partial V_S/\partial t < 0$ (lower
 583 left quadrant, Figure 11a), a similar $\bar{\zeta}_S/f$ sign transition occurs, with similar zero vor-
 584 ticity slope α , indicating a symmetric response with V_S sign change. South location vor-
 585 ticity recirculation is evident for $|\partial V_S/\partial t| > 0.3 \times 10^{-5} \text{ m s}^{-2}$. These observations demon-
 586 strate that previously generated $\bar{\zeta}/f$ can be advected back across the headland before
 587 significant vorticity generation can take place. This is consistent with oscillatory wake
 588 flow concepts and modeled tidal headland eddies of Signell & Geyer (1991).

589 At the west location, the relationship of $\bar{\zeta}_W/f$ to V_W and $\partial V_W/\partial t$ is qualitatively
 590 similar to the south location, with clear time-varying flow effects (Figure 11b). Compar-
 591 ing the south and west location, V_W is more often negative than V_S and $\bar{\zeta}_W/f$ is more
 592 strongly negative whereas $\bar{\zeta}_S/f$ is more strongly positive, consistent with Figures 6 and 10.
 593 As noted previously, for $V_W > 0$, the negative $\bar{\zeta}_W/f$ may be biased to low magnitudes
 594 (Appendix A). West location vorticity recirculation is not as clear as at the south loca-
 595 tion but is clearly evident for $\partial V_W/\partial t < -10^{-5} \text{ m s}^{-2}$. The zero vorticity slopes (6)
 596 are different as V_W changes sign with positive $\partial V_W/\partial t$ versus negative $\partial V_W/\partial t$ (com-
 597 pare upper-right to lower-left quadrants, respectively, in Figure 11b). As V_W becomes
 598 positive with positive $\partial V_W/\partial t$, the zero-vorticity slope is approximately $\alpha \approx 1/3600 \text{ s}^{-1}$
 599 (upper right dashed line in Figure 11b), about twice as steep as for the south location.
 600 As V_W becomes negative with negative $\partial V_W/\partial t$, the zero-vorticity slope $\alpha \approx 1/7200 \text{ s}^{-1}$
 601 (lower left dashed line in Figure 11b), similar to the south location. This implies an asym-
 602 metric $\bar{\zeta}_W/f$ response to V_W changing sign, with a much faster transition from south-
 603 ward to northward flow (upper right quadrant, Figure 11b) than from northward to south-
 604 ward flow (lower left quadrant, Figure 11b). This suggests asymmetry of vorticity gen-
 605 eration processes with different sign of mean flow at the west location, in particular, that
 606 negative vorticity may be rapidly generated as flow switches to northward.

607 **5 Asymmetric Vorticity Generation at the Headland**

608 The local vorticity-velocity relationship (Figure 10) suggests vorticity generation
 609 at the headland or farther upstream. Here, headland vorticity generation is inferred from
 610 estimates of the potential vorticity change across the headland (west and south locations).

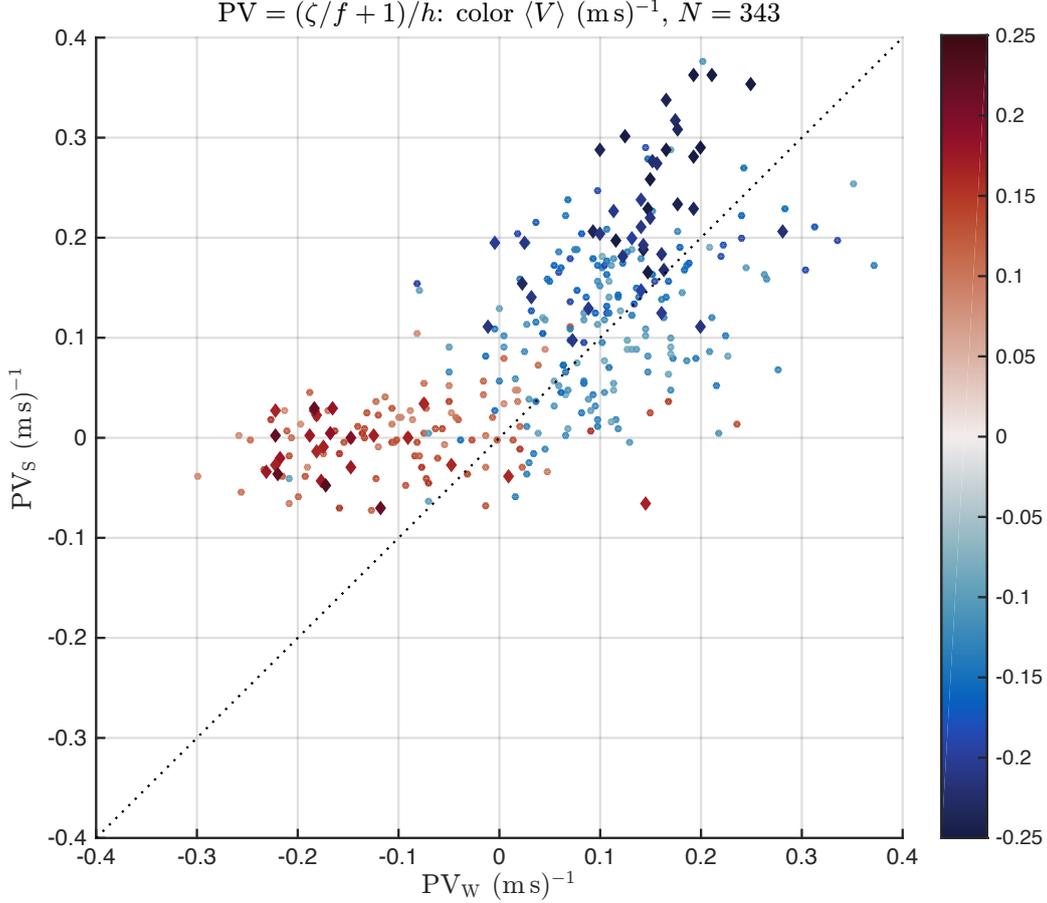


Figure 12. Potential Vorticity (PV) at the south (PV_S) location versus west (PV_W) location with symbols colored by the west and south averaged principal axes velocity $\langle V \rangle$ (10). Observations are limited quasi-steady conditions with $|\langle V \rangle| > 0.08 \text{ m s}^{-1}$ and $|\partial \langle V \rangle / \partial t| < 10^{-5} \text{ m s}^{-2}$, yielding 343 out of 928 hourly data points. Blue and red diamonds highlight data points where $\langle V \rangle \leq -0.2 \text{ m s}^{-1}$ (43 data points) and $\langle V \rangle \geq 0.16 \text{ m s}^{-1}$ (25 data points). Note, four data points lie outside the axes limits.

611 Potential vorticity PV is defined as

$$PV = \frac{\bar{\zeta}/f + 1}{h}, \quad (7)$$

612 and estimated at south and west locations with $h_S = 22.5 \text{ m}$ and $h_W = 19.0 \text{ m}$. In
613 an inviscid and homogeneous shallow water system, PV is conserved,

$$\frac{D(PV)}{Dt} = 0. \quad (8)$$

614 In a quasi-steady flow (*i.e.*, $\partial_t(PV)$ is small) and assuming that the west and south lo-
615 cations are upon the same streamline with uniform velocity, (8) simplifies to

$$PV_S = PV_W. \quad (9)$$

616 With bottom friction, potential vorticity can be generated, and deviations from (9) be-
617 tween upstream and downstream locations can be interpreted as headland PV genera-

618 tion, under the above assumptions. Here, we address potential vorticity generation at
 619 the Pt. Sal headland by comparing PV_W to PV_S as a function of south and west loca-
 620 tion averaged principal axes velocity $\langle V \rangle$ defined as

$$\langle V \rangle = \frac{1}{2}(V_S + V_W). \quad (10)$$

621 As the analysis of PV generation assumes quasi-steady conditions, we limit observations
 622 to times when $|\partial\langle V \rangle/\partial t| < 10^{-5} \text{ m s}^{-2}$ and $|\langle V \rangle| > 0.08 \text{ m s}^{-1}$ based on Figure 11.
 623 Recall that V_S and V_W were highly correlated with $r = 0.86$ (Figure 6b). The results
 624 below are not dependent on the chosen $\langle V \rangle$ and $\partial\langle V \rangle/\partial t$ cutoffs.

625 The relationship between PV_S and PV_W as a function of $\langle V \rangle$ is shown in Figure 12.
 626 For southward flow $\langle V \rangle < -0.08 \text{ m s}^{-1}$, both PV_W and PV_S are generally both posi-
 627 tive and increase with more negative $\langle V \rangle$ (blue colors in Figure 12), although occasion-
 628 ally PV at one or both locations is also negative. When both PV_S and PV_W are posi-
 629 tive with $\langle V \rangle < -0.08 \text{ m s}^{-1}$, no clear trend above or below the 1:1 line is evident and
 630 a best-fit to those data yield a slope slightly < 1 . However, for the strongest southward
 631 flow $\langle V \rangle < -0.2 \text{ m s}^{-1}$, nearly all 43 data points have $PV_S > PV_W$ by a factor of $1.5\times$
 632 to $2\times$ (diamonds in Figure 12). Under the above assumptions (steady and on a stream-
 633 line), this suggests that headland vorticity (PV) generation is weak for relatively weak
 634 southward flow (and implies vorticity generation upstream of the west location), but sig-
 635 nificant PV generation occurs for stronger southward flow.

636 For northward flow $\langle V \rangle > 0.08 \text{ m s}^{-1}$ (red colors in Figure 12), PV generation is
 637 clearly indicated under the above assumptions. At the upstream (south) location for $\langle V \rangle >$
 638 0.08 m s^{-1} , PV_S is generally small within $\pm 0.1 \text{ (m s)}^{-1}$ with a near-zero mean. Over-
 639 all, $PV_S < 0$ is uncommon (see also the uncommon $\bar{\zeta}_S/f < -1$ in Figure 7). Most of
 640 the corresponding PV_W are negative, varying between -0.3 and 0 (m s)^{-1} and are sub-
 641 stantially more negative than PV_S . For larger $\langle V \rangle > 0.16 \text{ m s}^{-1}$ (red diamonds in Fig-
 642 ure 12), PV_W is generally more negative (mean of -0.14 (m s)^{-1}) whereas $PV_S \approx 0$.
 643 This suggest that for northward flow, on average, substantial PV is generated at the head-
 644 land. Note that for northward flow, the negative $\bar{\zeta}_W$ is likely biased to low magnitudes
 645 (Appendix A) and that $\bar{\zeta}_W$ and thus PV_W is likely even more negative. The difference
 646 between northward and southward flow suggests asymmetry in headland vorticity gen-
 647 eration.

648 6 Discussion

649 6.1 Phase space of different flow time-scales

650 Steady flow concepts indicate strong vorticity generation for northward flow and
 651 weak vorticity generation only for stronger southward flow. For realistic time-dependent
 652 flows, Pt. Sal vorticity depends upon V and $\partial V/\partial t$ (Figure 11), consistent with pure pe-
 653 riodic flow concepts. At Pt. Sal, the depth-averaged principal axes V is composed of semi-
 654 diurnal, diurnal, and subtidal ($> 33 \text{ h}$) flow time-scales that move through V and $\partial V/\partial t$
 655 phase space. Here, lower and higher frequency flows movement through $(V, \partial V/\partial t)$ phase
 656 space (ellipses in Figure 11) in relation to vorticity recirculation and generation is ex-
 657 amined using a periodic velocity

$$V(t) = V_0 \cos(\omega t), \quad (11)$$

658 for semidiurnal (12.42 h period, ω_{sd}) or a subtidal (72 h period, ω_{st}) radian frequencies
 659 corresponding to the dominant variability of V (Figure 6b). The subtidal radian fre-

660 quency corresponding to 72 h is chosen as a representative subtidal frequency. The semi-
 661 diurnal and subtidal velocity amplitude both are assigned $V_0 \approx 0.12 \text{ m s}^{-1}$ correspond-
 662 ing to the semidiurnal spring tide amplitudes and subtidal velocity amplitude (std times
 663 $\sqrt{2}$). For periodic flow, the vorticity adjustment time-scale t_α is the time to go from $V =$
 664 0 to crossing the zero-vorticity ($\bar{\zeta}/f = 0$) slope $\alpha = \partial V/\partial t/V$ defined as,

$$t_\alpha = \omega^{-1} \cot^{-1} \left(\frac{\alpha}{\omega} \right), \quad (12)$$

665 and for $\alpha/\omega \ll 1$, $t_\alpha \rightarrow \alpha^{-1}$. The advective recirculation distance L_α over the vortic-
 666 ity adjustment time-scale t_α is approximately,

$$L_\alpha = V_0 \omega^{-1} [1 - \cos(\omega t_\alpha)]. \quad (13)$$

667 For subtidal (72 h) flow, the phase space ellipse is eccentric with relatively weak
 668 accelerations ($< 4 \times 10^{-6} \text{ m s}^{-2}$, Figure 11 dotted ellipse), implying that $\bar{\zeta}/f$ is pre-
 669 dominantly a function of V . The subtidal orbital excursion amplitude $V_0/\omega_{\text{st}} \approx 5000 \text{ m}$,
 670 greater than the separation between the west and south locations ($L_{\text{W,S}} \approx 1200 \text{ m}$).
 671 At subtidal periods, the $\bar{\zeta}/f = 0$ slope for $\alpha = (1/7200) \text{ s}^{-1}$ is crossed in $t_\alpha = 2 \text{ h}$,
 672 allowing only $L_\alpha \approx 75 \text{ m}$ of recirculated vorticity prior to the V sign switch, substan-
 673 tially less than $L_{\text{W,S}} \approx 1200 \text{ m}$. For $\alpha = (1/3600) \text{ s}^{-1}$ the vorticity adjustment time-
 674 scale $t_\alpha \approx 1 \text{ h}$, and the recirculation distance $L_\alpha = 19 \text{ m}$ is even shorter. Subtidal
 675 velocity variability is often red, and using subtidal periods longer than 72 h in (12) and
 676 (13) results in even shorter recirculation distances.

677 For semidiurnal oscillatory flow, the accelerations are much stronger, up to $1.7 \times$
 678 10^{-5} m s^{-2} , resulting in $\bar{\zeta}/f$ that depends on both V and $\partial V/\partial t$ (Figure 11, solid ellipse).
 679 The semidiurnal orbital excursion amplitude $V_0/\omega_{\text{sd}} \approx 850 \text{ m}$ is less than $L_{\text{W,S}} \approx 1200 \text{ m}$.
 680 For $\alpha = (1/7200) \text{ s}^{-1}$, the semidiurnal vorticity adjustment time-scale $t_\alpha = 1.5 \text{ h}$, with
 681 $L_\alpha = 250 \text{ m}$ of recirculation. For semidiurnal flow and $\alpha = (1/3600) \text{ s}^{-1}$, the recircu-
 682 lation distance is even smaller $t_\alpha = 1 \text{ h}$ and $L_\alpha = 92 \text{ m}$.

683 The recirculation distances for subtidal ($L_\alpha = 75 \text{ m}$) and semidiurnal ($L_\alpha = 250 \text{ m}$)
 684 are small relative to the ≈ 1200 separation between W and S centroid locations. In a
 685 time-varying paradigm, vorticity switching sign before a water parcel could advect a dis-
 686 tance $L_{\text{W,S}}$ (Figure 11) suggests consistent headland vorticity generation for both north-
 687 ward and southward flow even at semidiurnal time-scales. This is consistent with the steady-
 688 flow paradigm of inferred PV generation for northward flow (red in Figure 12) and for
 689 stronger southward flow (blue diamonds). However, for southward flow, the steady-flow
 690 paradigm only suggested PV generation for strong southward flow (blue diamonds in Fig-
 691 ure 12). This difference may reflect a limitation of the assumptions of steady flow on a
 692 streamline in the potential vorticity analysis (Section 5). Flow variability at Pt. Sal is
 693 dominated by semidiurnal and lower frequency variability. Although the actual $(V, \partial V/\partial t)$
 694 phase space path involves a range of time-scales, all semidiurnal and longer time-scales
 695 will give $L_\alpha < L_{\text{W,S}}$. As a vorticity adjustment time-scale is evident at the south lo-
 696 cation for $|\partial V_{\text{S}}/\partial t| > 0.3 \times 10^{-5} \text{ m s}^{-2}$, these conclusions apply to any time-scale present
 697 in the flow with sufficient acceleration magnitude.

698 6.2 Dimensional and non-dimensional parameter space

699 Here, we contextualize Pt. Sal relative to other observed headland and island wakes
 700 in both dimensional and non-dimensional parameter space. Pt. Sal has characteristic length-
 701 scale $L \sim 1 \text{ km}$ (Figure 1) consistent with TTP (*e.g.*, MacCready & Pawlak, 2001) and
 702 the Zandmotor (Radermacher et al., 2017), but considerably smaller than Velasco Reef,

703 Palau $L \sim 10$ km (MacKinnon et al., 2019). Note, the Zandmotor is a low sloped (low
 704 aspect ratio) feature, in contrast to the sharp (high aspect ratio) features of Pt. Sal, TTP,
 705 and Velasco Reef. The Pt. Sal characteristic depth $h \sim 20$ m is similar to the Zand-
 706 motor ($h \sim 10$ m), but much shallower than the 200 m and 600 m depths of TTP and
 707 Velasco Reef (MacCready & Pawlak, 2001; MacKinnon et al., 2019). The Coriolis pa-
 708 rameter $f = 8.3 \times 10^{-5} \text{ s}^{-1}$ is characteristic of mid-latitudes, but is four times larger
 709 than that for the near-equatorial Palau ($f = 2.1 \times 10^{-5} \text{ s}^{-1}$). The Pt. Sal principal
 710 axes currents are broadband (Figure 6b) similar to Velasco Reef (MacKinnon et al., 2019)
 711 contrasting with the primarily tidal flow of TTP and Zandmotor. Based on the variance
 712 in each of the semidiurnal and subtidal bands, the velocity scale is $U \sim 0.12 \text{ m s}^{-1}$ for
 713 each and a total of $U \sim 0.2 \text{ m s}^{-1}$. This is similar to TTP ($U_0 \sim 0.2 \text{ m s}^{-1}$), weaker
 714 than the semidiurnal tidal velocity at Velasco Reef ($U_0 \sim 0.4 \text{ m s}^{-1}$), and substantially
 715 weaker than the Zandmotor ($U_0 \sim 0.7 \text{ m s}^{-1}$). The sea-bed near Pt. Sal is generally
 716 composed of medium grain sand, and a bulk quadratic drag coefficient $C_D = 2 \times 10^{-3}$
 717 is used for depth-averaged flow. This embeds the surface gravity wave enhanced bottom
 718 stress within C_D (Feddersen et al., 2000; Lentz et al., 2018). Note that near Pt. Sal, the
 719 bed is rocky reef with large roughness. The semidiurnal (12.42 h) radian frequency $\omega_{\text{sd}} \approx$
 720 $1.4 \times 10^{-4} \text{ s}^{-1}$. The subtidal time-scale is broadband but here as above we ascribe a
 721 72 h subtidal radian frequency $\omega_{\text{st}} = 2.4 \times 10^{-5} \text{ s}^{-1}$.

722 In terms of non-dimensional parameters, we estimate the Pt. Sal Rossby number
 723 ($\text{Ro} = U/fL$) with the full $U \sim 0.2 \text{ m s}^{-1}$ resulting in $\text{Ro} \sim 2.4$, a value near Velasco
 724 Reef and TTP ($\text{Ro} \sim 0.9$, $\text{Ro} \sim 2$, respectively MacKinnon et al., 2019; Canals et al.,
 725 2009), and smaller than Zandmotor $\text{Ro} \sim 6.1$ (Radermacher et al., 2017). Note, the Ve-
 726 lasco Reef near-one Ro is due to both the much larger L and a smaller f than Pt. Sal.
 727 The Pt. Sal frictional Reynolds number ($\text{Re}_f = h/C_D L$) is estimated as $\text{Re}_f \sim 10$, which,
 728 as TTP and Velasco reef are in deep water, can only be compared to Zandmotor at $\text{Re}_f \sim$
 729 5 . As the flow has multiple time-scales (*i.e.*, broadband), estimating the ratio of flow ex-
 730 cursion to headland length scale $K_c = U_0/(\omega L)$ is challenging. Here we use the spring-
 731 tide $U_0 = 0.12 \text{ m s}^{-1}$ and ω_{sd} to estimate a semi-diurnal $K_c^{(\text{sd})} \sim 0.85$, indicating that
 732 that vorticity can be weakly recirculated over a tidal cycle. The Pt. Sal $K_c^{(\text{sd})}$ is substan-
 733 tially smaller than the $K_c^{(\text{sd})} \sim 5.0$ of the Zandmotor, but similar to $K_c^{(\text{sd})} = 1.4$ of TTP,
 734 and substantially larger than the $K_c^{(\text{sd})} = 0.14$ of Velasco Reef. The Pt. Sal $K_c^{(\text{sd})}$ re-
 735 sults in $\text{Re}_f/K_c^{(\text{sd})} \sim 12$ suggesting that the vorticity decay time-scale is longer than a
 736 semidiurnal period. As the vorticity adjustment time-scale $t_\alpha < 2$ h (Section 6.1, Fig-
 737 ure 11), this further suggests that vorticity generation at the headland is dominant. In
 738 contrast, the Zandmotor $\text{Re}_f/K_c^{(\text{sd})} \sim 1$ consistent with the headland eddy decaying within
 739 a tidal time-scale (Radermacher et al., 2017).

740 Here, we have examined depth-averaged vorticity and flow at Pt. Sal and neglected
 741 stratification effects. In other headland vorticity generation regions, stratification is im-
 742 portant. The Pt. Sal time-average buoyancy frequency $N \sim 0.016 \text{ s}^{-1}$, estimated from
 743 the mean top-to-bottom temperature differences at the thermistor moorings near Pt. Sal,
 744 and the local deformation radius $L_d \sim 3.8$ km leads to a Burger number of $L_d/L \sim$
 745 3.8 . The buoyancy frequency (stratification) at TTP ($N \sim 0.01 \text{ s}^{-1}$) and Velasco Reef
 746 ($N \sim 0.02 \text{ s}^{-1}$) are similar, leading to much larger Burger number at TTP $L_d/L =$
 747 18 and Velasco Reef $L_d/L = 50$. Thus, the vorticity generated at Pt. Sal will adjust
 748 to geostrophy more rapidly than at TTP and Velasco Reef. Note, no stratification was
 749 reported for the ZandMotor. At both TTP and Velasco Reef, the Froude number regime
 750 allows for both internal lee waves as well as vorticity generation (Warner & MacCready,
 751 2014; Voet et al., 2020). For flow traveling past Pt. Sal, no coherent obstacle is present
 752 (Figure 3), that would allow for lee wave generation even with the strong stratification.

753 7 Summary

754 As part of the Inner Shelf Dynamics Experiment (Kumar et al., 2020), two months
 755 of fixed ADCP velocity measurements in ~ 20 m depth near the asymmetric headland
 756 Pt. Sal CA are used to investigate headland vorticity generation and recirculation. Pt. Sal
 757 is a sharp (120° bend) rocky headland with scale of ~ 1 km. To reduce vorticity esti-
 758 mation noise, ADCP velocities were low-pass filtered with a 2 h time-scale and were re-
 759 constructed from the first two EOF modes that represented $\approx 73\%$ of the variance. Depth-
 760 averaged vorticity was estimated at two locations west and south of Pt. Sal from the smoothed
 761 reconstructed velocities of groups of fixed ADCPs. Only one west-location vorticity com-
 762 ponent was estimated, leading to negative vorticity bias for northward flow. Vorticity
 763 was also estimated from multiple parallel vessel transects on a single day. The observed
 764 depth-averaged flow principal axes velocity V was primarily along-bathymetric contours
 765 and varied largely between ± 0.2 m s^{-1} across subtidal, diurnal, and semidiurnal frequency
 766 bands. At west and south locations, the V was well correlated at $r = 0.86$. The south
 767 location vorticity is consistent with vorticity estimated from parallel vessel transects on
 768 a single day. The vorticity variability was vertically coherent and primarily depth-uniform.

769 Vertical vorticity kinematics and dynamics were studied with the depth averaged
 770 vorticity $\bar{\zeta}/f$. At west and south locations, the depth-averaged normalized vorticity $\bar{\zeta}/f$
 771 varied ± 8 across subtidal, diurnal, semidiurnal, and supertidal frequency bands, had more
 772 high frequency variability than V , and was less correlated ($r = 0.55$) than for V . The
 773 vorticity distributions are skewed with opposite sign at west and south locations. Neg-
 774 ative PV ($\bar{\zeta}/f < -1$) is more likely at both locations than open ocean suggesting strong
 775 vorticity generation. At west and south locations, $\bar{\zeta}/f$ and V were related, but asym-
 776 metrically with sign of V , indicating vorticity generation at the headland or farther up-
 777 stream. Analysis within both steady flow and time-varying flow paradigms indicates asym-
 778 metric vorticity generation across the headland. Binned-mean $\bar{\zeta}/f$ depends on both V
 779 and $\partial V/\partial t$, and indicates vorticity recirculation across the headland as V switches sign.
 780 The time-scale for vorticity adjustment is ~ 2 h, and the associated short excursion dis-
 781 tances indicate generation between south and west locations, with stronger generation
 782 at west location for the transition to northward flow. For quasi-steady flow, the south
 783 and west potential vorticity relationship indicates asymmetric vorticity generation be-
 784 tween the south and west locations, with stronger vorticity generation for northward flow.
 785 The inferred asymmetric vorticity generation for northward flow is consistent with $\bar{\zeta}/f <$
 786 -1 more likely at the west location than south location. Pt. Sal occupies a portion of
 787 non-dimensional parameter space that is unique relative to other well studied headlands.

788 Appendix A Vorticity estimation bias at west location

789 As $\bar{\zeta}_W$ was estimated from two ADCPs, only one component of vertical vorticity
 790 $\partial\tilde{v}/\partial\tilde{x}$ was calculated and $\partial\tilde{u}/\partial\tilde{y}$ was neglected, where (\tilde{y}, \tilde{v}) represents the principal axes
 791 direction and flow magnitude, respectively (Section 2.2.2). In Sections 4 and 5, $\bar{\zeta}_W$ is an-
 792 alyzed in the context of headland generation or unsteady-flow induced recirculation. How-
 793 ever, these results could instead be due to noise and bias in the $\bar{\zeta}_W$ estimation method.
 794 Here, potential biases in west location vorticity estimates are qualitatively examined us-
 795 ing characteristic examples southward and northward flow (Figure A1) and implications
 796 for results are discussed.

797 First consider southward flow from 13-Sept-2017 12:00PDT (Figure A1a), one hour
 798 after the vessel survey concluded (Figure 9). South ADCP (green squares) depth-averaged
 799 velocities bend (or rotate) south to south east while velocity decreases from 9 cm s^{-1} to

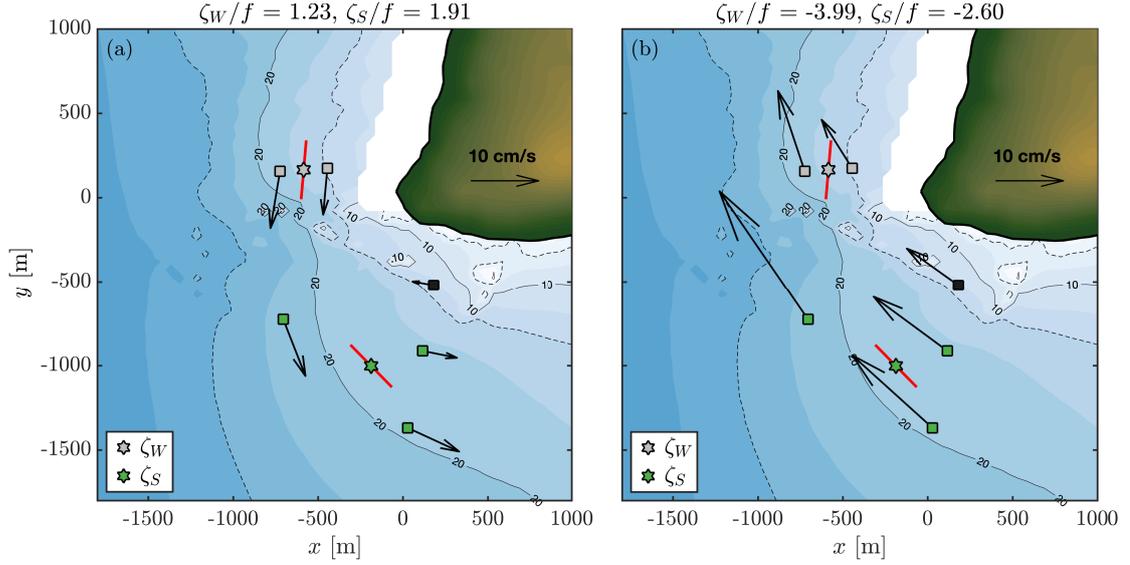


Figure A1. Depth-averaged velocity examples near Pt. Sal to illustrate west location vorticity bias: (a) Southward flow on 13-Sept-2017 12:00 PDT with $\bar{\zeta}_W/f = 1.23$ and $\bar{\zeta}_S/f = 1.91$ and (b) Northward flow on 28-Sept-2017 12:00 PDT with $\bar{\zeta}_W/f = -3.99$ and $\bar{\zeta}_S/f = -2.60$. Squares represent ADCP locations and black arrows represent depth-averaged velocities. Stars are vorticity estimation locations and the red line gives the orientation of the fit-velocity principal axes. Gray and green markers represent west and south ADCPs and vorticity estimation locations, respectively (see also Figure 3). The solid and dashed lines represent the 15, 20, and 25 m depth contours.

800 5 cm s^{-1} with decreasing depth, giving a sense of positive vorticity. Both components
 801 of vorticity ($\partial\bar{v}/\partial\bar{x}$ and $\partial\bar{u}/\partial\bar{y}$) are important to the estimated $\bar{\zeta}_S/f = 1.91$. The west
 802 ADCPs (gray squares in Figure A1a) have a southward, roughly along-isobath, $7\text{--}9 \text{ cm s}^{-1}$
 803 depth-averaged flow in the principal axes direction with larger magnitude at the offshore
 804 location, suggesting positive vorticity. The west estimated $\bar{\zeta}_W/f = 1.23$ using only $\partial\bar{v}/\partial\bar{x}$
 805 (Section 2.2.2). At this time, the west velocities perpendicular to the principal axes di-
 806 rection are weak with ADCP averaged $\bar{u} = 0.4 \text{ cm s}^{-1}$, much smaller than character-
 807 istic \bar{v} . An ADCP farther upstream (north) in the principal axes direction would likely
 808 have near-zero depth-averaged onshore flow (*i.e.*, $\bar{u} \approx 0$) due to the coastline bound-
 809 ary. This would on average lead to $|\partial\bar{u}/\partial\bar{y}| \ll |\partial\bar{v}/\partial\bar{x}|$ for southward flow. Thus, $\bar{\zeta}_W$
 810 may have unbiased error that the statistical analysis of Sections 4 and 5 reduces, we ar-
 811 gue that the bias is weak for southward flow.

812 The northward flow example (Figure A1b) suggests potential northward flow bias
 813 in the west location vorticity due to west location cross-principal axis flow. At the south
 814 ADCP (green squares), the flow is to the NW at $13\text{--}23 \text{ cm s}^{-1}$ in the principal axes di-
 815 rection (red line at green star). The depth-averaged flow variation parallel and perpen-
 816 dicular to the principal axes direction both suggest negative vorticity, and the estimated
 817 $\bar{\zeta}_S/f = -2.60$ using both components of vorticity. At the west location (gray squares
 818 in Figure A1b), the depth-averaged flow is also NW at $9\text{--}13 \text{ cm s}^{-1}$ with faster flow off-
 819 shore. However, the depth-averaged velocities are not aligned with the principal axis di-

820 rection (red line at gray star), with the ratio of cross-axis to along-axis velocity \tilde{u}/\tilde{v} ra-
 821 tio of 0.75 and 0.43 at shallow and deeper west ADCP locations, respectively. The $\partial\tilde{v}/\partial\tilde{x}$
 822 estimated $\bar{\zeta}_W/f = -3.99$ is larger than the $\bar{\zeta}_S/f$ estimate, suggesting vorticity gener-
 823 ation, but is likely biased by not including $\partial\tilde{u}/\partial\tilde{y}$. To constrain the sign of the bias, con-
 824 sider an ADCP farther to the north in the lee of Pt. Sal along the principal axis direc-
 825 tion. This ADCP would likely have $\tilde{u} \approx 0$ as depth-averaged onshore flow is limited by
 826 the boundary (as for southward flow) and $\partial\tilde{u}/\partial\tilde{y}$ would be positive. Thus, the true vor-
 827 ticity $\bar{\zeta}_W = \partial\tilde{v}/\partial\tilde{x} - \partial\tilde{u}/\partial\tilde{y}$ would be even more negative. In this case, if west ADCP
 828 $\tilde{u}/\tilde{v} = 0.5$ and $\partial\tilde{y} = \partial\tilde{x} = 280$ m, then $\bar{\zeta}_W/f \approx -6$. For northward flow, we qualita-
 829 tively argue that the $\bar{\zeta}_W$ estimate is positively biased, and that the true west vorticity
 830 is even more negative than estimated. Thus, the inference of strong potential vorticity
 831 generation for northward flow (Section 5) is likely accurate but the generation rate is un-
 832 derestimated.

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